


REINHOLD ENVIRONMENTAL Ltd.



2016 NO_x-Combustion-CCR Round Table Presentation

February 1 & 2, 2016, in Orlando, FL / Hosted by OUC

All presentations posted on this website are copyrighted by Reinhold Environmental, Ltd (RE). Any unauthorized downloading, attempts to modify or to incorporate into other presentations, link to other websites, or obtain copies for any other uses than the training of attendees to RE's Conferences is expressly prohibited, unless approved in writing by RE or the original presenter. RE does not assume any liability for the accuracy or contents of any materials contained in this library which were presented and/or created by persons who were not employees of RE.



Orlando, FL
February 2, 2016

Broaden the Operating Range of Coal Fired Units by Lowering the Minimum Operating Temperature

Reinhold Environmental 2016 NO_x-Combustion-CCR Round Table



Volker Rummenhohl

Agenda

- Introduction
- Basics of SCR Minimum Operating Temperature (MOT)
- Variety of solutions to reduce MOT
- Conclusions

Introduction

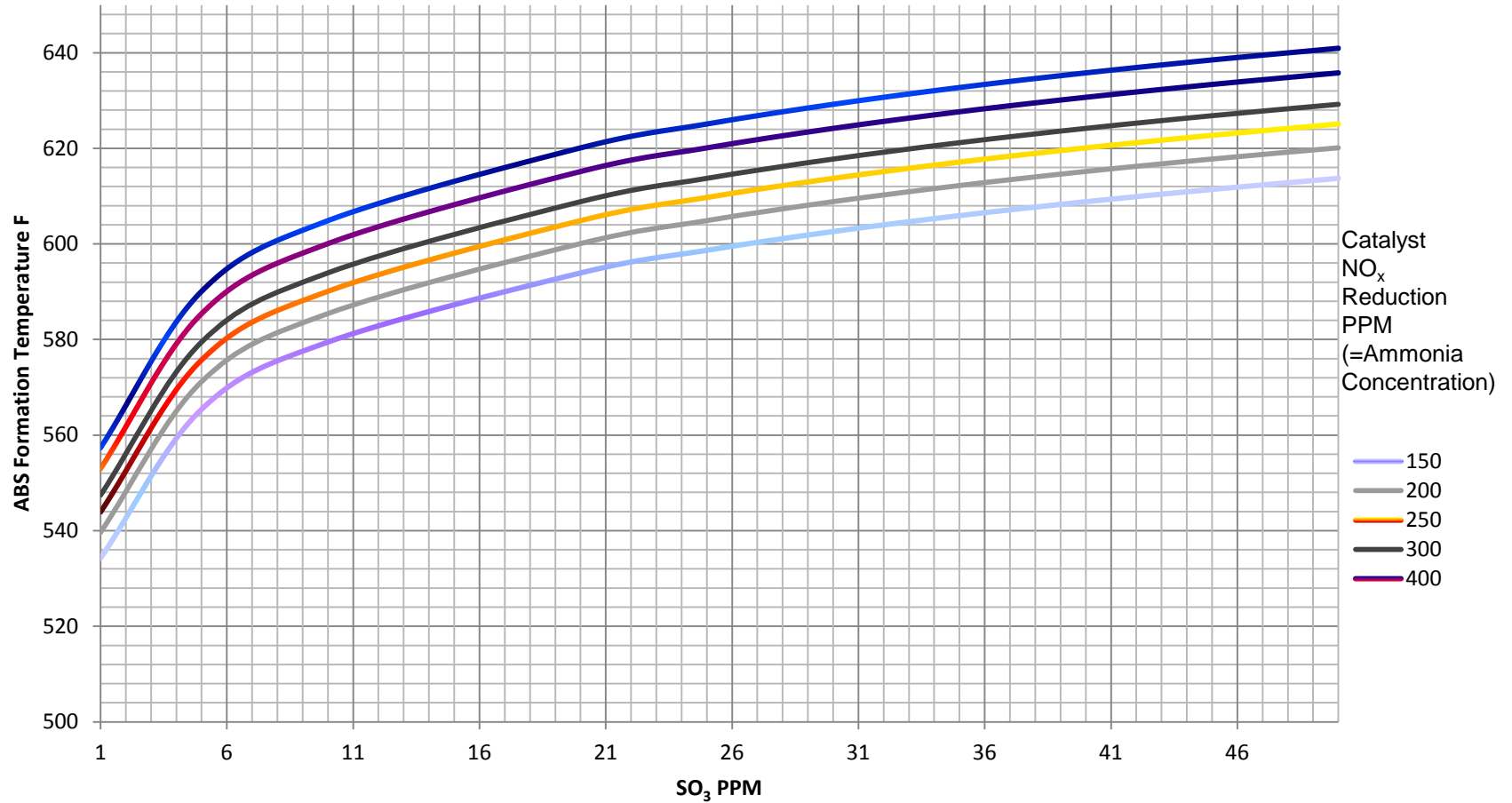
- Improving unit dispatch in an ever changing coal electricity generation market place requires the lowest possible unit load.
- The boiler is often limited by the Minimum Operating Temperature of the SCR system.



MOT

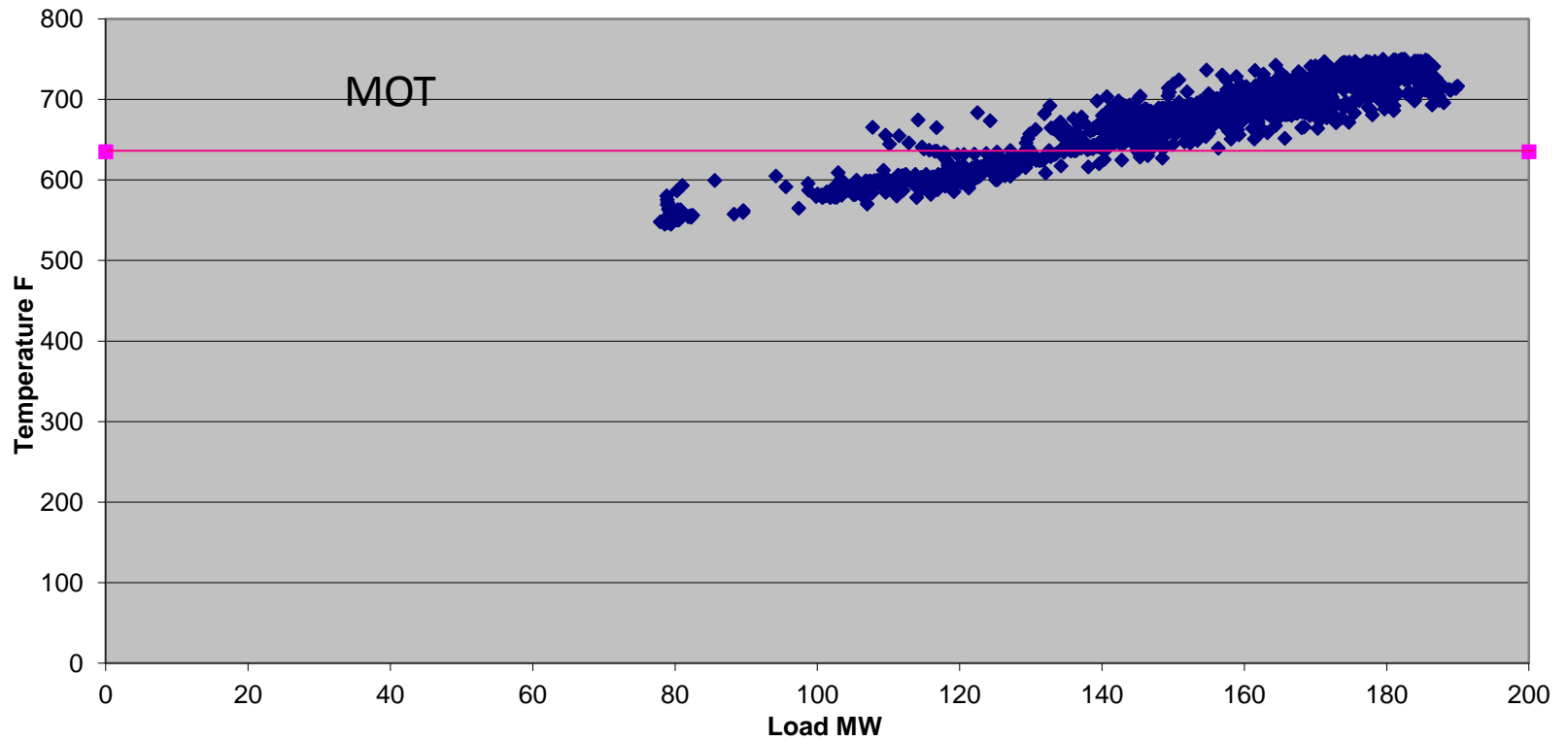
- The Minimum Operating Temperature is the temperature below which ammonia and sulfur trioxide combine to form ammonium bisulfate (ABS).
- $\text{NH}_3 + \text{SO}_3 + \text{H}_2\text{O} \longrightarrow \text{NH}_4\text{HSO}_4$
- ABS deposits in the micro pores and reduces the catalyst activity.
- The ABS deposits can be removed at higher temperatures.
- The MOT depends on the NH_3 and SO_3 concentration in the flue gas.

Example



Economizer Temperature Characteristic

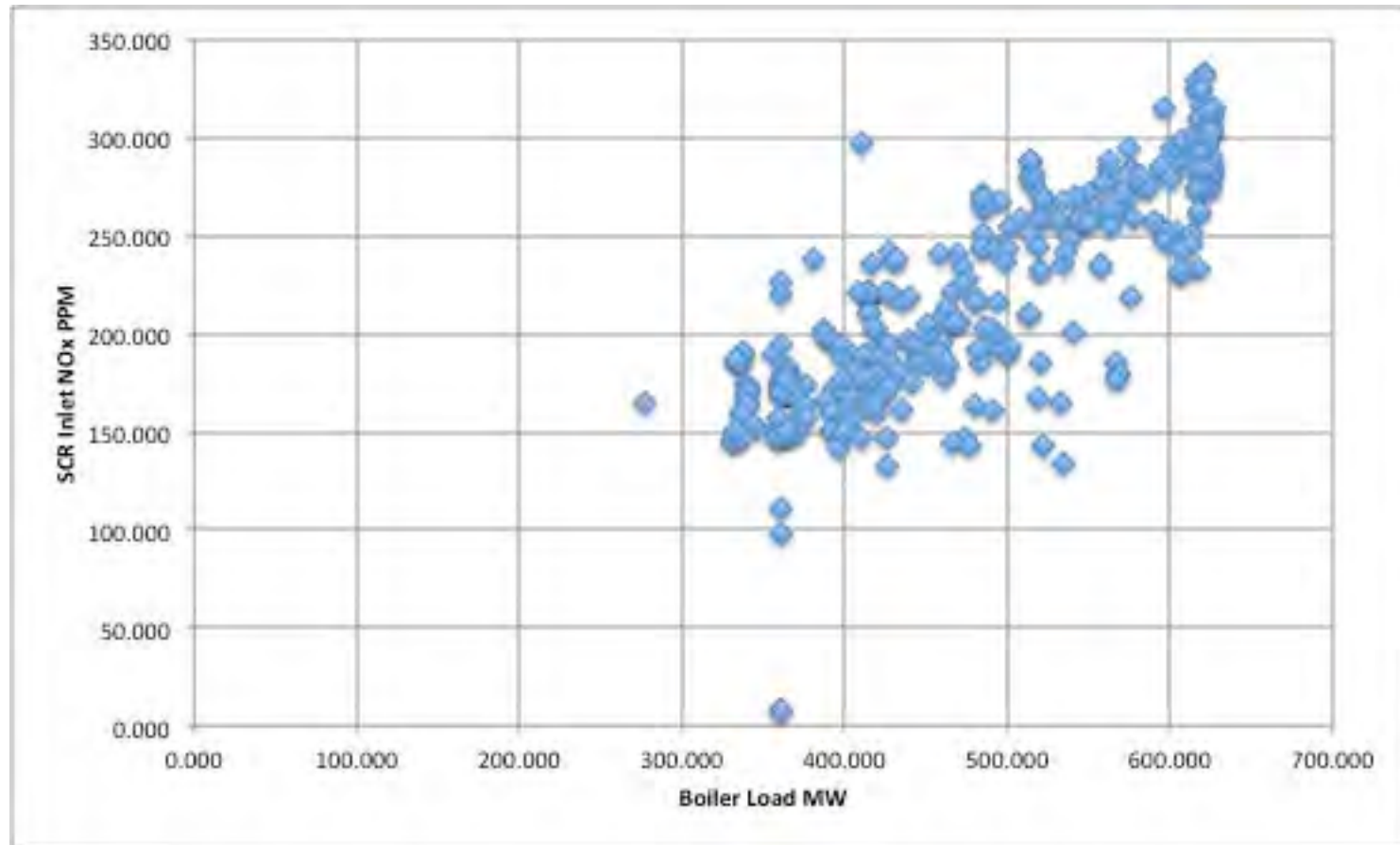
Temperature VS Load



Solutions

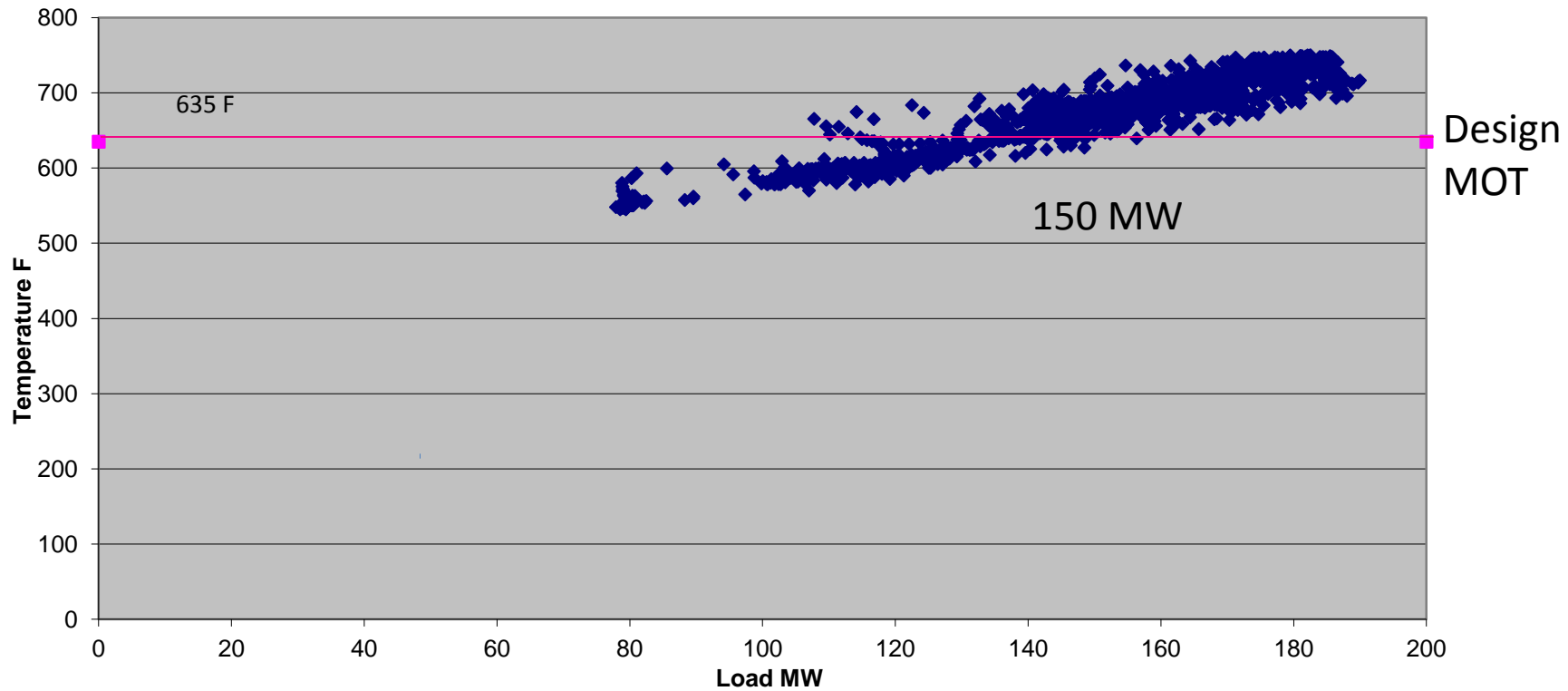
- Verify operating data at low loads
- Operate below MOT
- Increase economizer outlet temperature
- Reduce ammonia concentration in the flue gas
- Reduce sulfur trioxide concentration in the flue gas
- Combination of the above

NO_x VS Load



Economizer Temperature Characteristic

Temperature VS Load

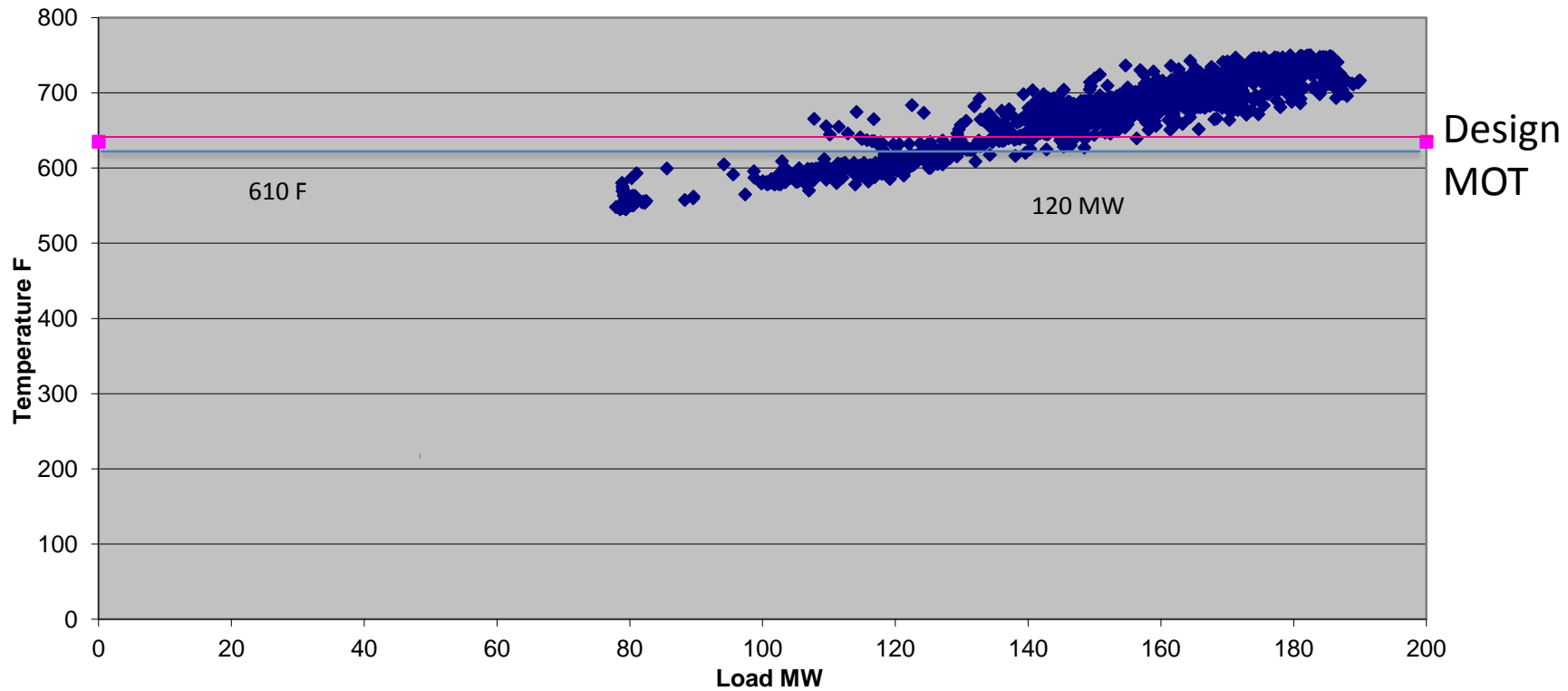


Verification of Low Load Operating Data

- NO_x inlet
- NO_x distribution
- SO₂ inlet
- SO₂ distribution
- SO₃ inlet
- SO₃ distribution
- Temperature inlet
- Temperature distribution
- Ammonia slip

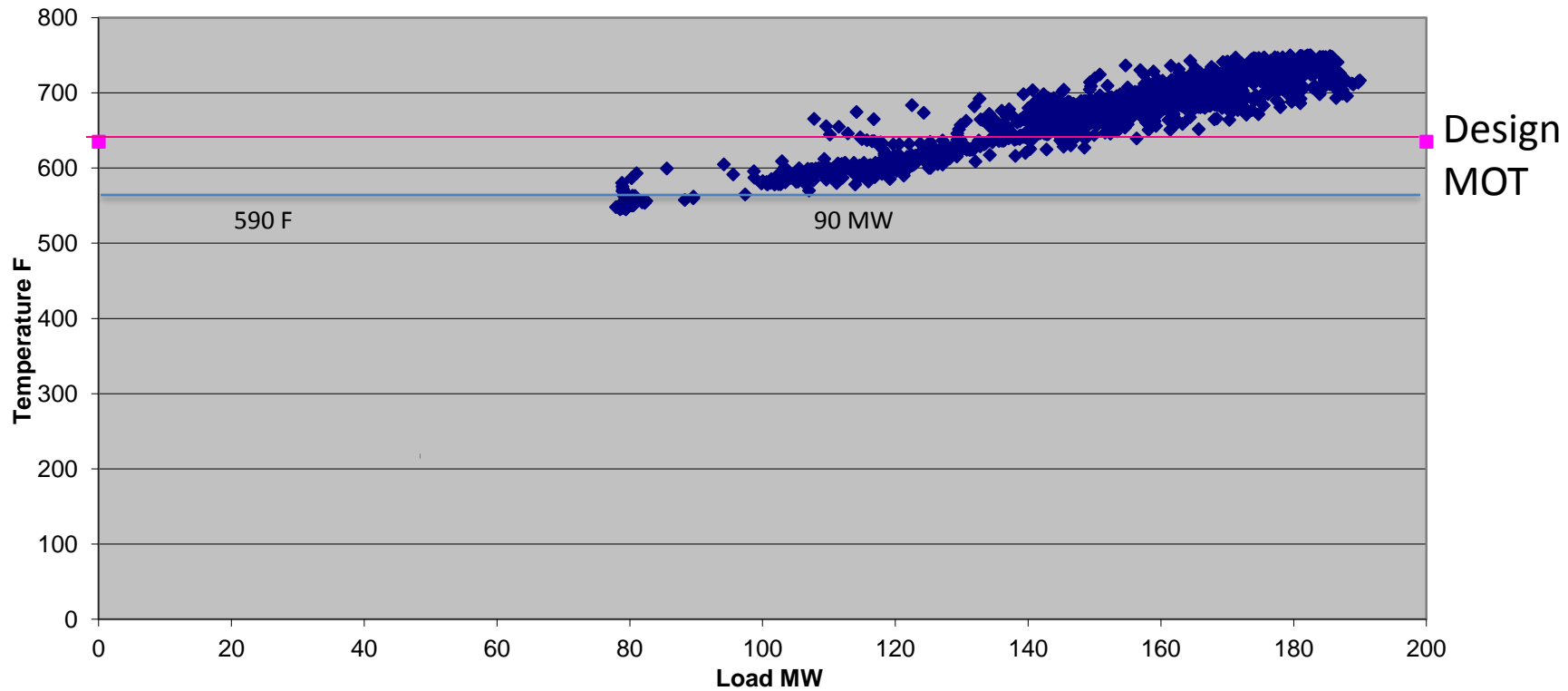
Verification of Low Load Operating Data

Temperature VS Load



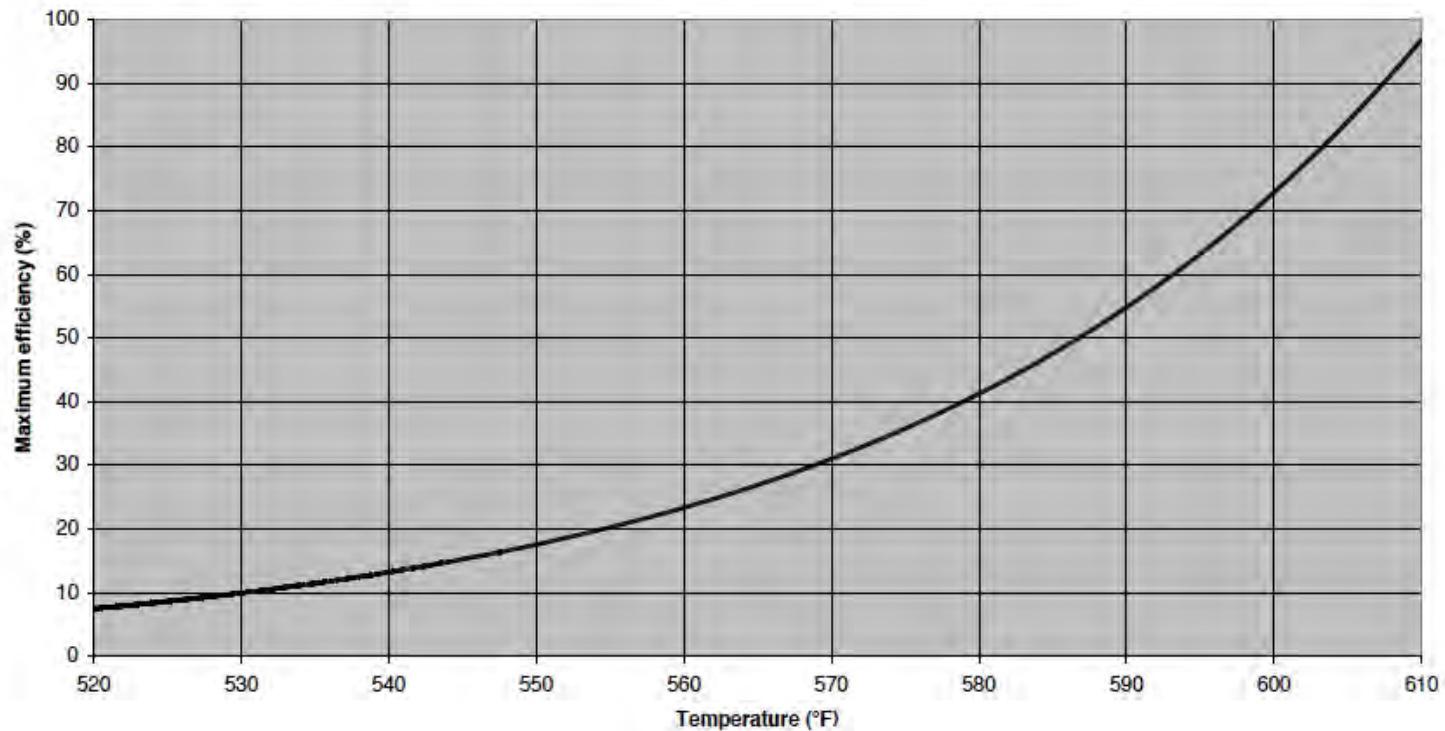
Verification of Low Load Operating Data

Temperature VS Load



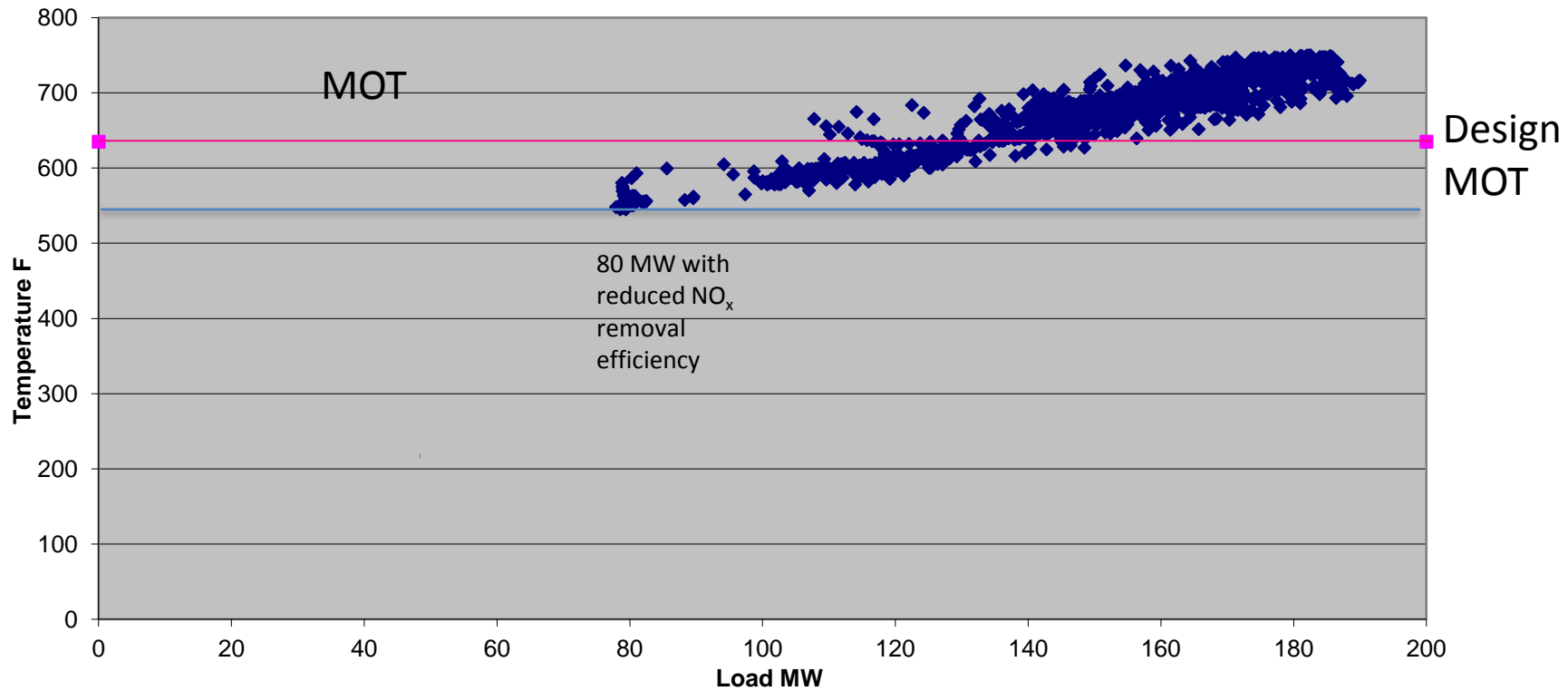
Reduce Ammonia concentration

Maximum efficiency (%) vs Temperature
NOx Inlet concentration: 300 ppm
SO3 concentration : 15 ppm



Economizer Temperature Characteristic

Temperature VS Load



Operation Below MOT

- Deterioration of Ammonia/NO_x profile inside the catalyst mostly on high sulfur units
- Time dependent
- Other sulfite formation

Operating Below MOT on High Sulfur Unit

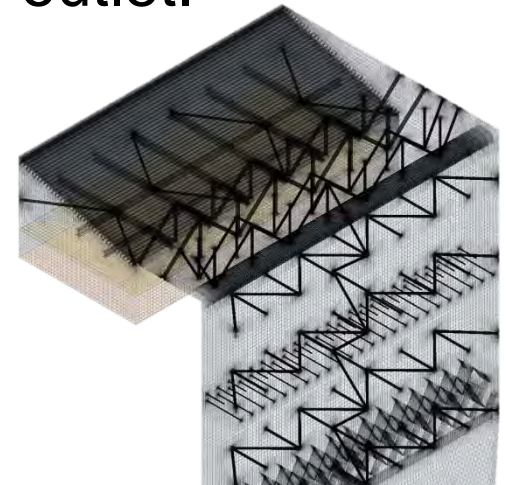
- 500 MW unit wall fired
- Bituminous coal with 3% sulfur
- Full load performance test
 - Guaranteed NO_x removal exceeded
 - Ammonia slip not detectable
 - NO_x outlet distribution +/- 10 PPM
- Low load Second performance test
 - Guaranteed NO_x removal exceeded
 - Ammonia slip 2 PPM
 - NO_x outlet distribution +/- 20 PPM

Operating Below MOT on High Sulfur Unit

- Low load first performance test
 - As full load test
- Low load second performance test
 - Guaranteed NO_x removal exceeded
 - Ammonia slip 2 PPM
 - NO_x outlet distribution +/- 20 PPM
- Low load third performance test
 - Guaranteed NO_x removal exceeded
 - Ammonia slip 10 PPM
 - NO_x outlet distribution +/- 50 PPM

Bio Mass Unit

- SCR clean side arrangement (444°F) - downstream of baghouse and DSI.
- Most catalyst poisons have condensed on ash and removed in bag house.
- DSI removes 70-90% of SO_x
- Minimum operating temperature of 423°F based on design SO_2 / SO_3 values at baghouse outlet.
- Additional design constraints:
 - Ammonia Slip <5ppmvd @ 7% O_2
 - 2 year initial lifetime guarantee
 - Catalyst pressure drop <1.2" wg



Bio Mass Unit

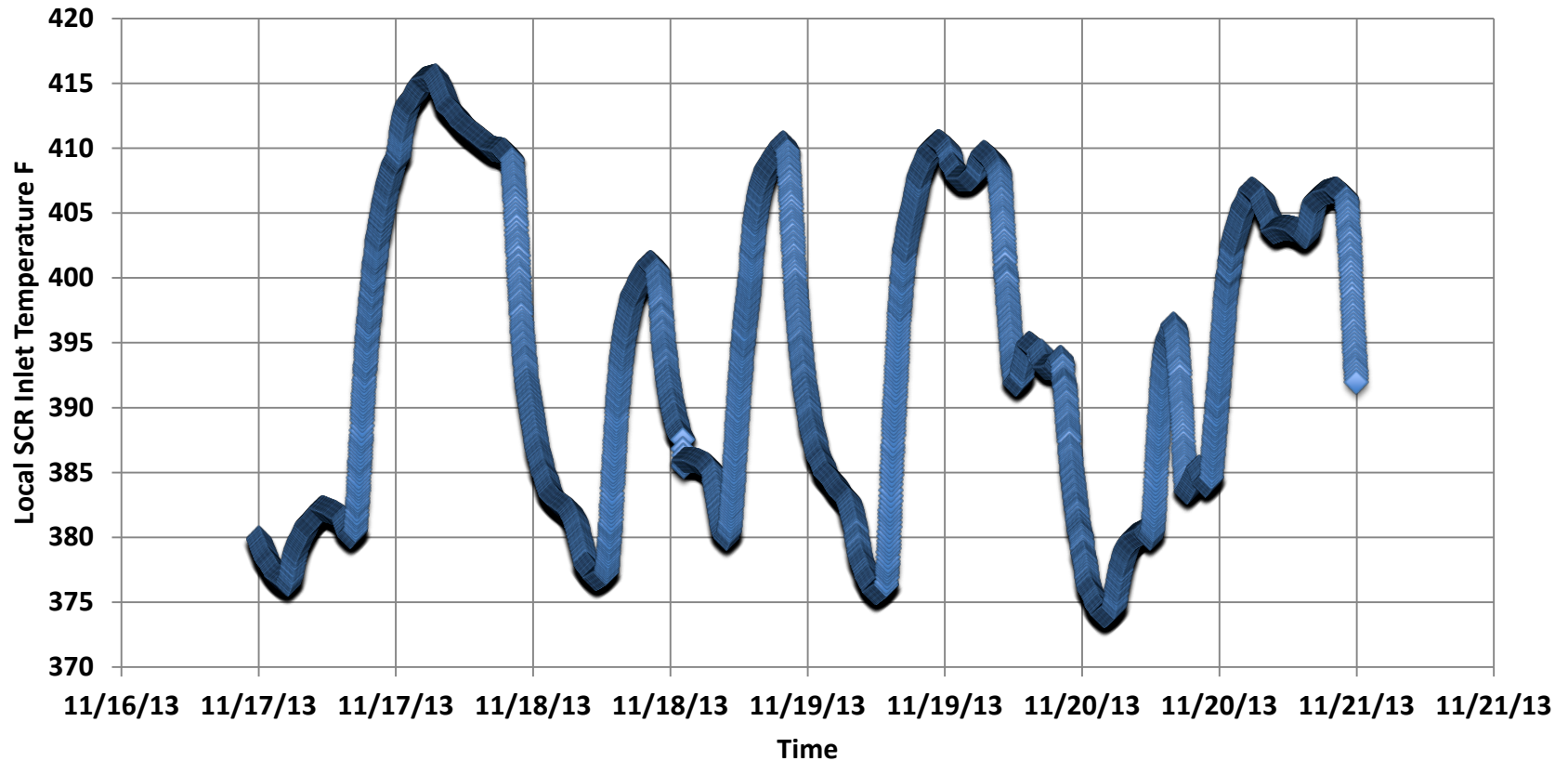
- Boiler first fire July 7, 2013
- SCR Baseline testing began on November 19, 2013.
- NO_x removal set point target set at 0.078 lb/MMBTU and met.
- Ammonia slip testing done at a set point of 0.045 lb/MMBTU. Set point was met and no ammonia slip excursions found.
- Initial compliance emissions testing results, November 2013:
 - NO_x: 0.052 lb/MMBtu
 - Ammonia slip: 0.7 ppmvd @ 7% O₂

Bio Mass Unit

Current Operation

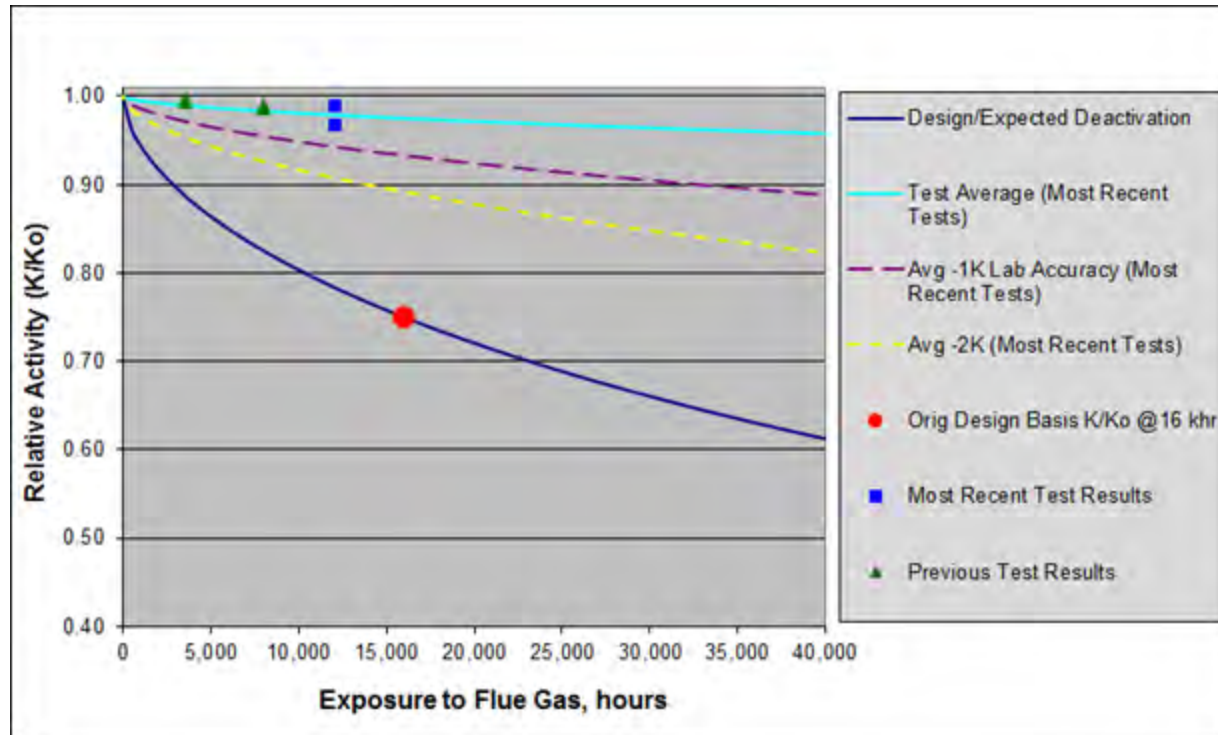
- NO_x Inlet 0.138 - 0.155 lb/MMBTU
- NO_x Outlet 0.032 - 0.075 lb/MMBTU
- Temperature 375°F - 423°F
- Pressure Drop (SCR) less than 2" Wg

Operation Below MOT

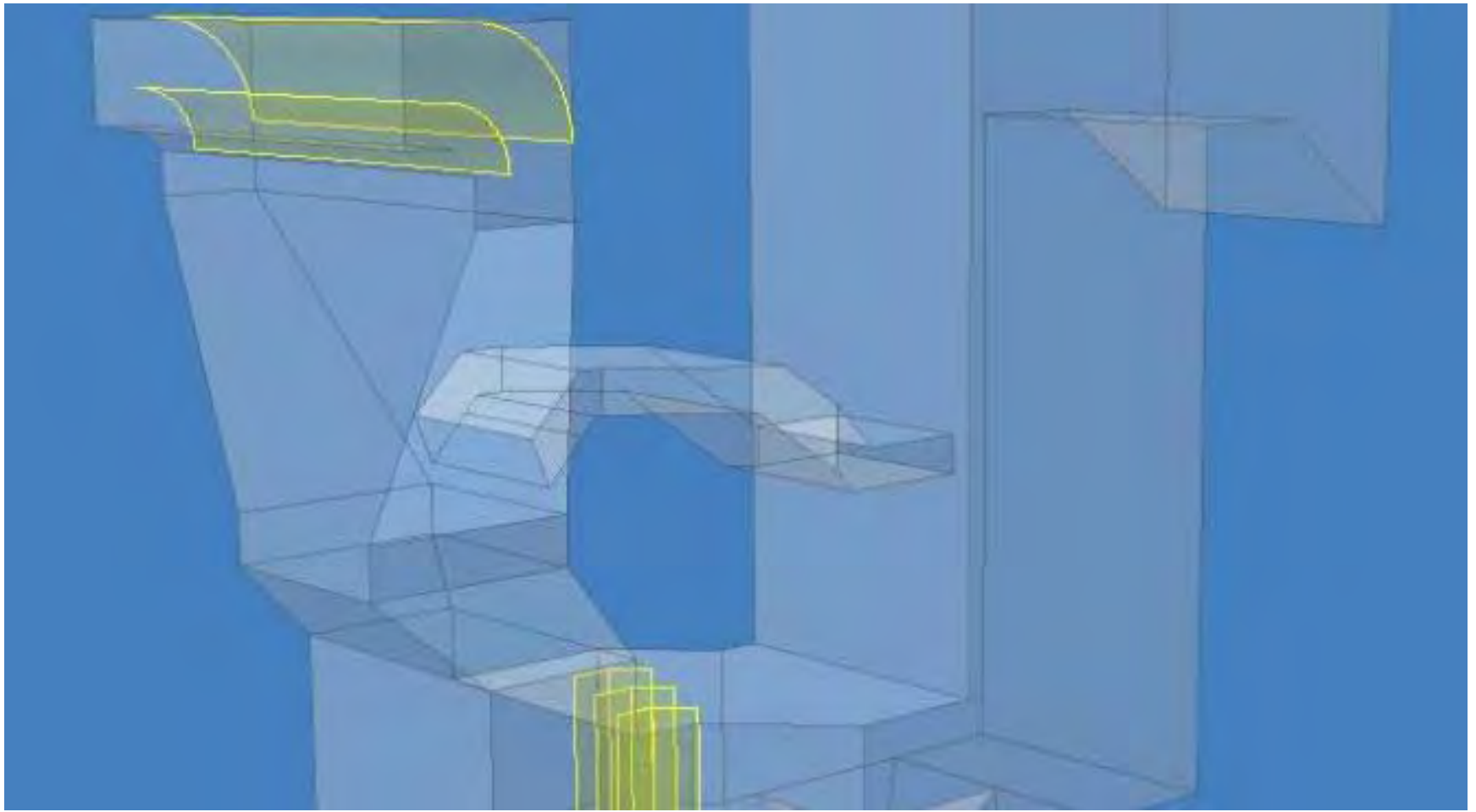


Bio Mass Unit

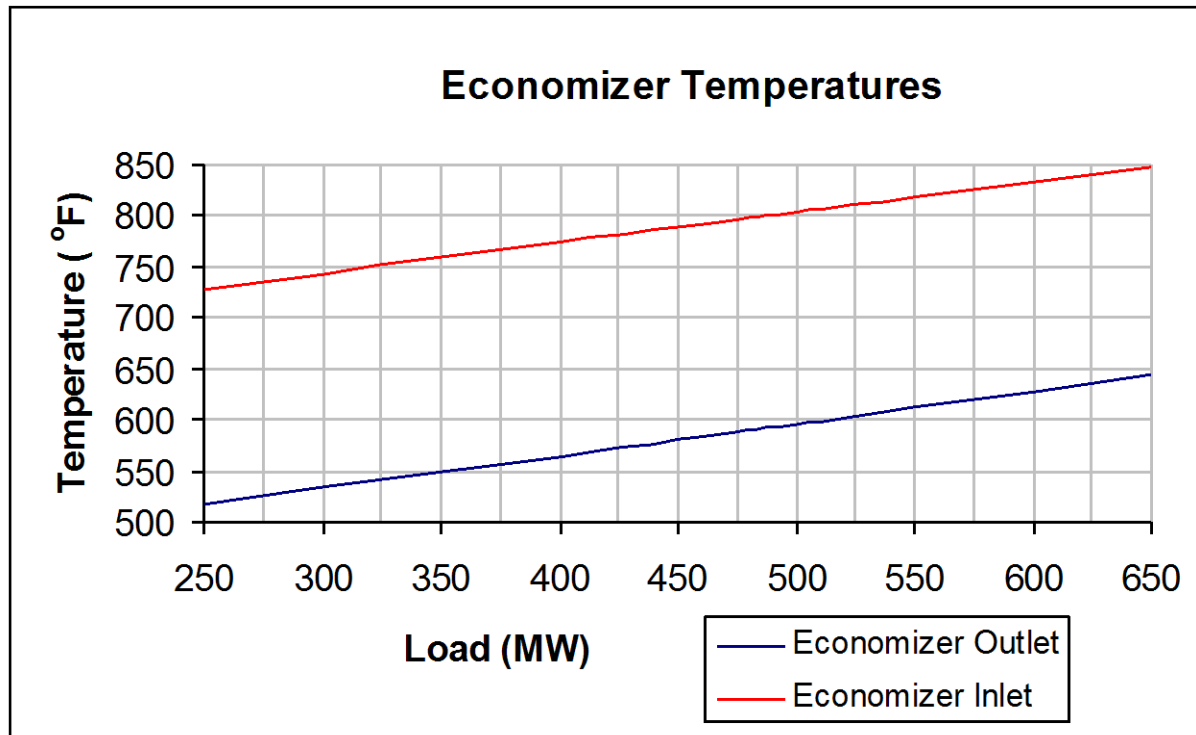
- Testing done at 4,000 and 8,000 hours



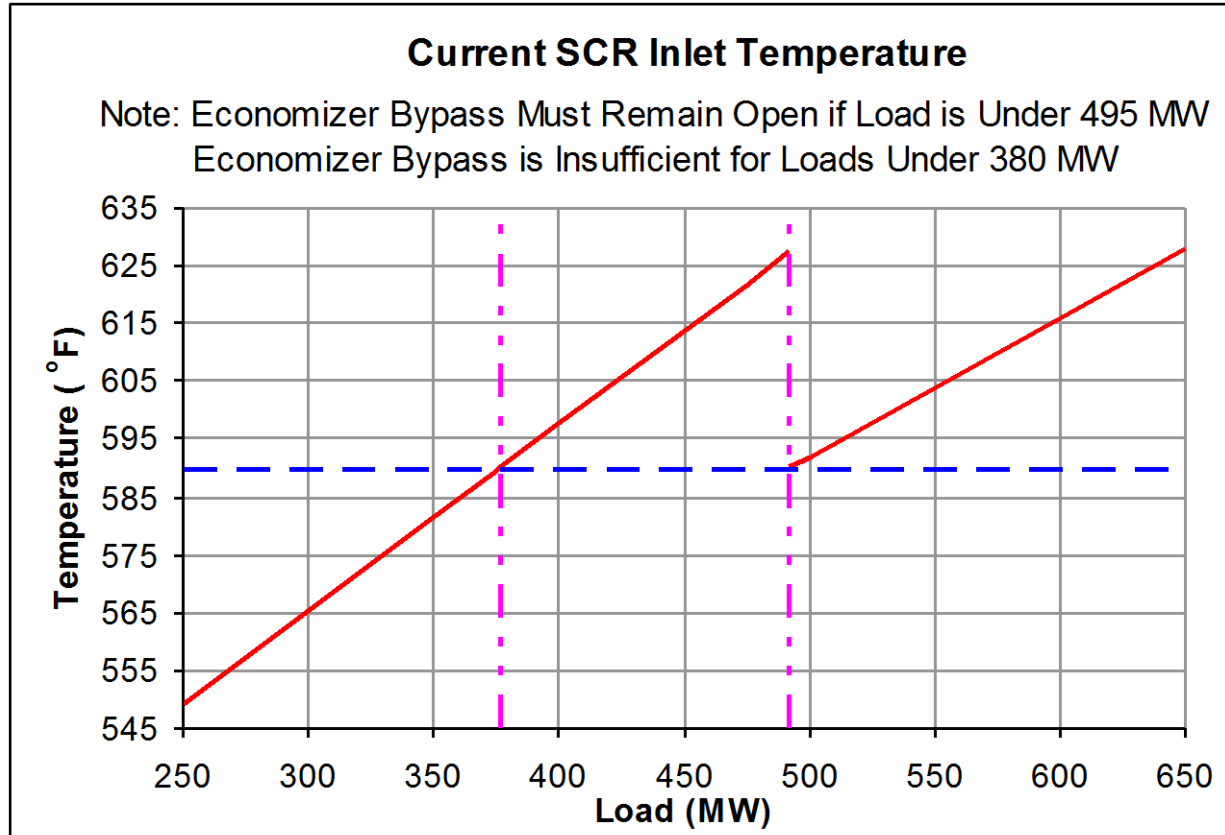
Economizer Gas Side Bypass



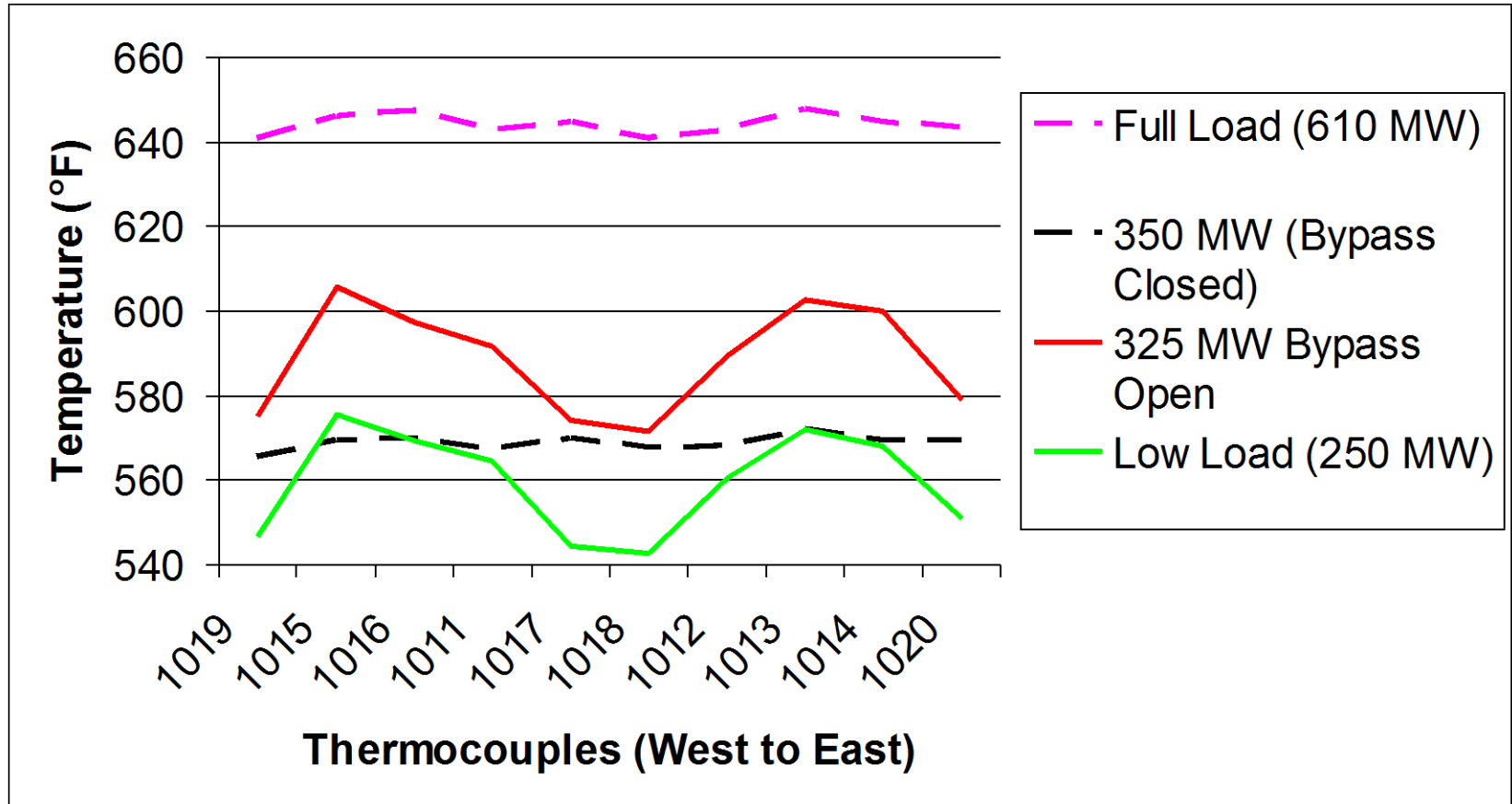
Economizer Gas Side Bypass



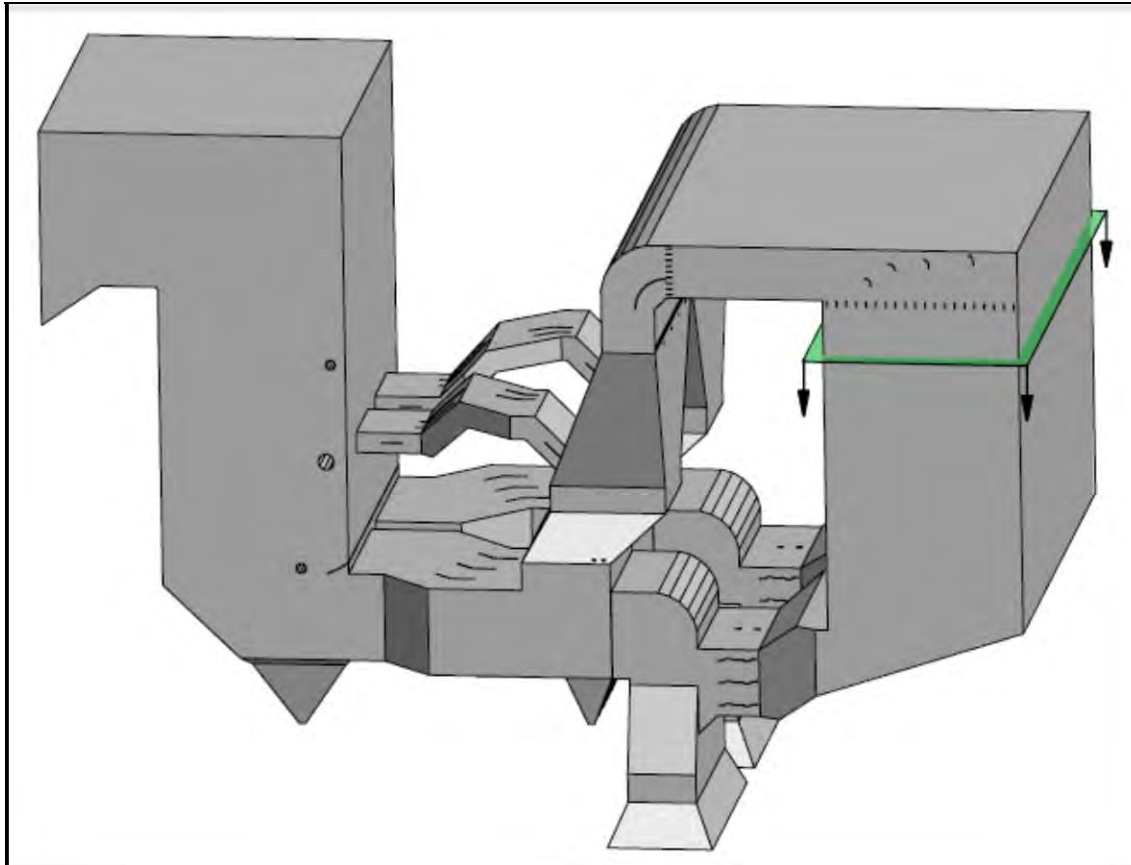
Economizer Gas Side Bypass



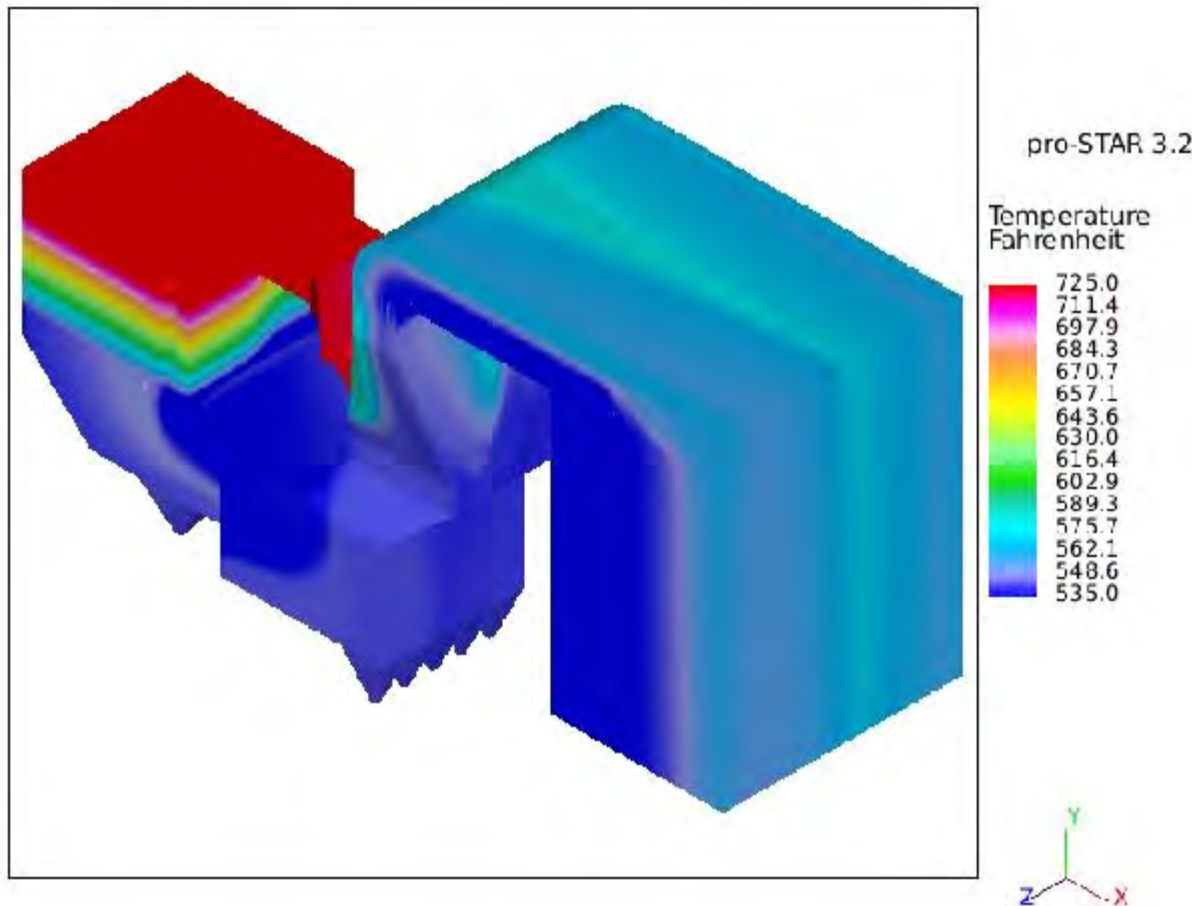
Economizer Gas Side Bypass



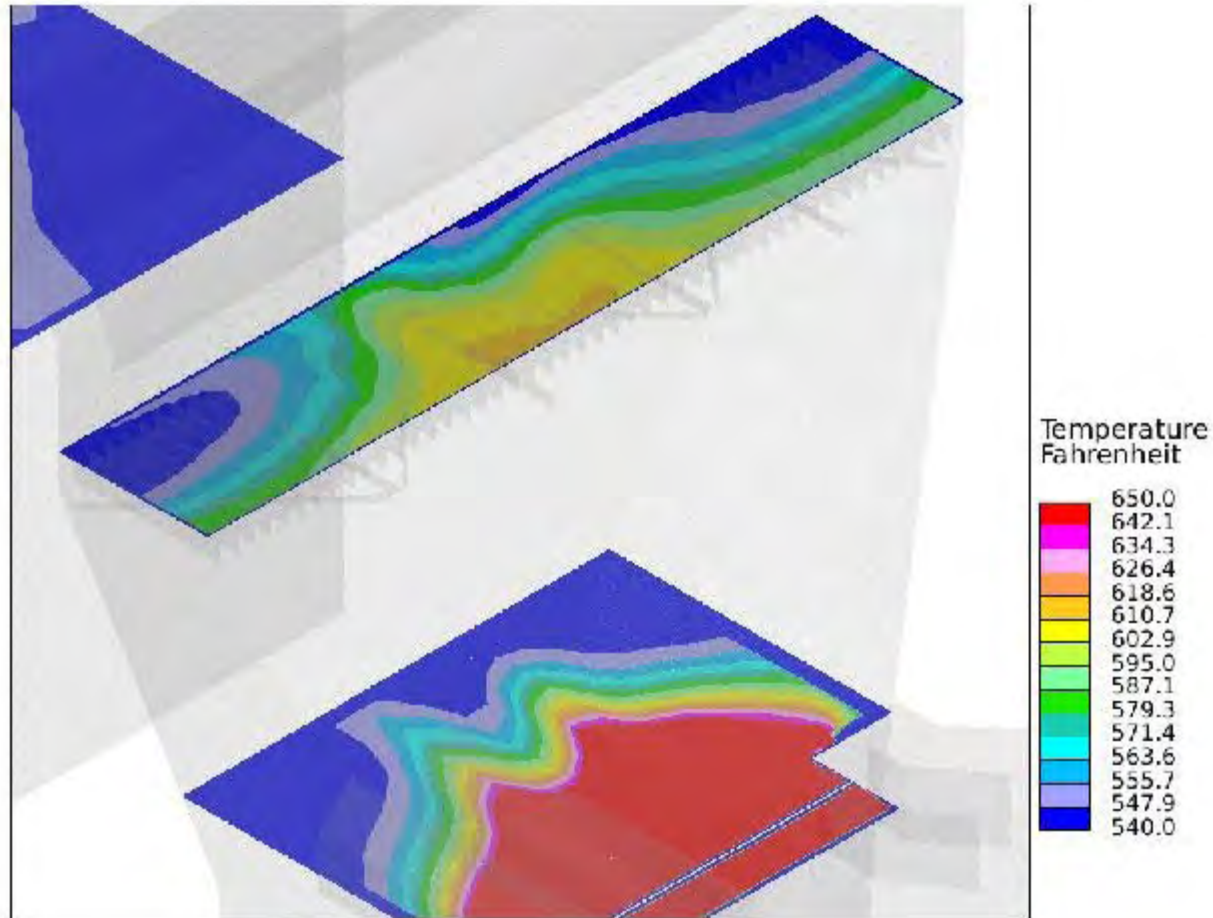
Economizer Gas Side Bypass



Economizer Gas Side Bypass

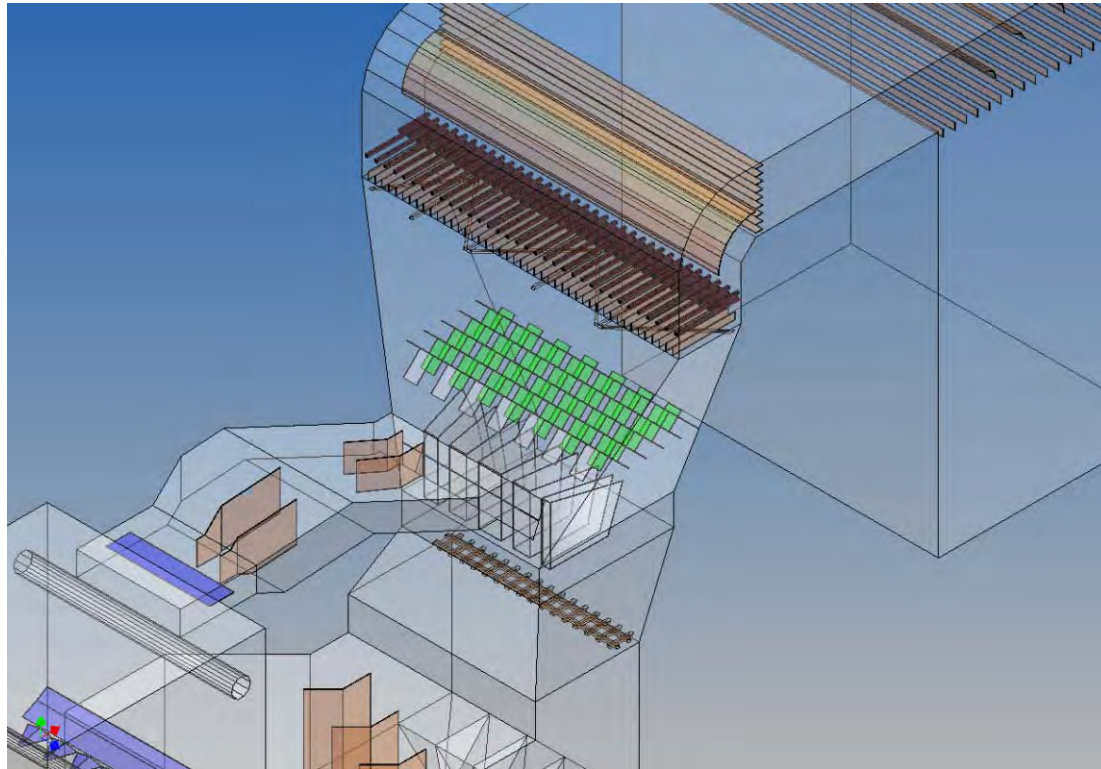


Economizer Gas Side Bypass



Economizer Gas Side Bypass

Possible Solution

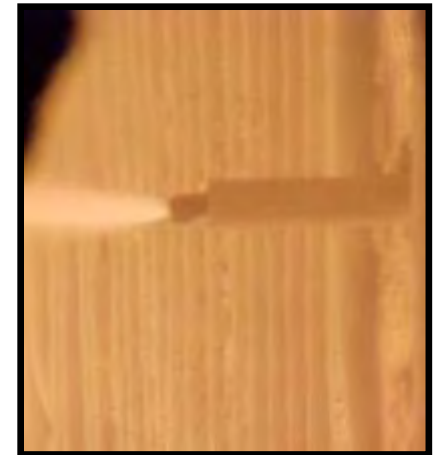


Economizer Water Side Bypass

- Pro: No flue gas mixing issues
- Con: Many times difficult to retrofit
- No flow water flow through part of the economizer

SO₃ Reduction With Targeted In-Furnace Injection TIFI

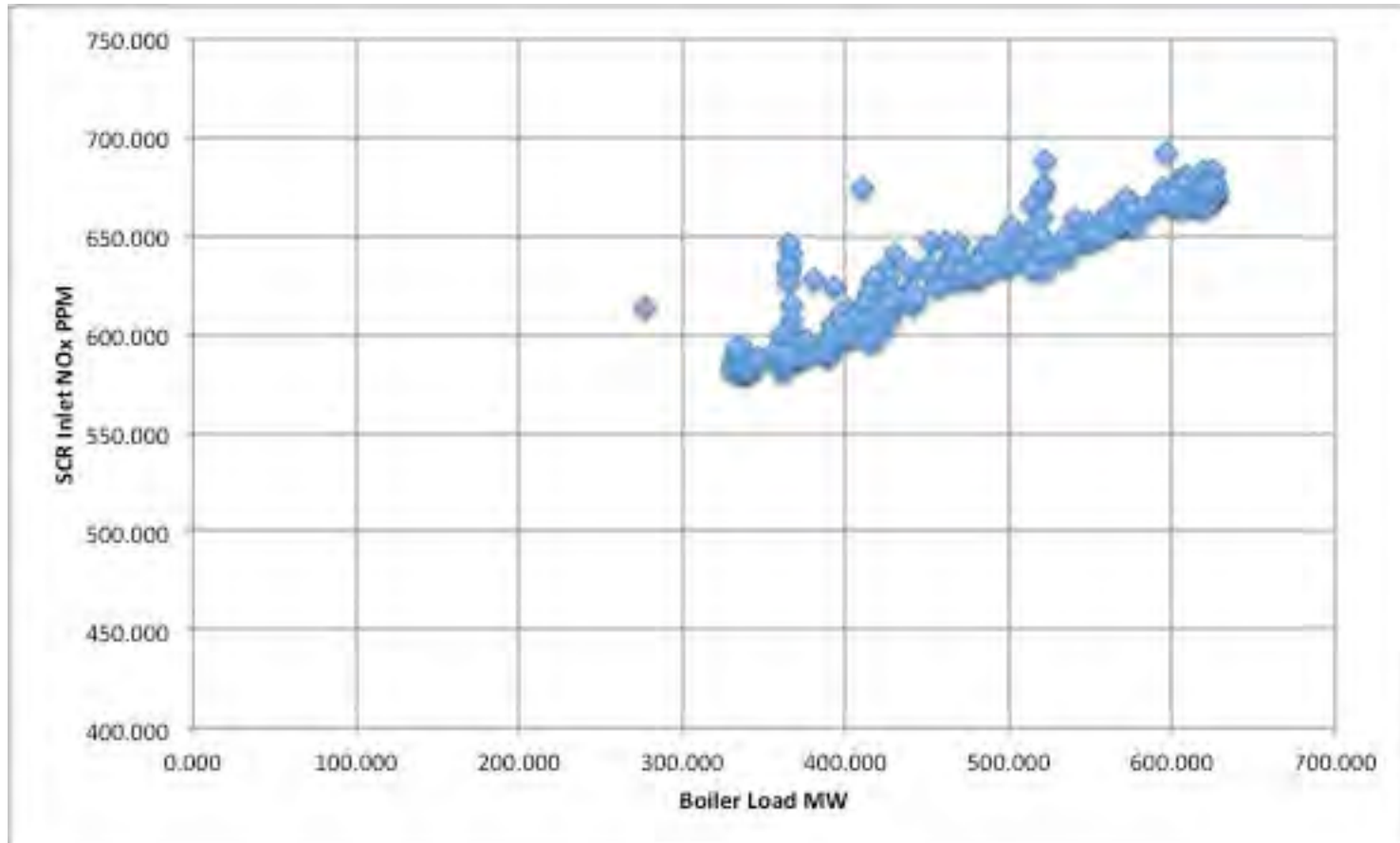
- Mg(OH)₂ calcines to high surface area MgO
- Direct Reaction with MgO
 - $\text{MgO} + \text{SO}_3 \Rightarrow \text{MgSO}_4$
 - $\text{MgO} + \text{NH}_4\text{HSO}_4 \Rightarrow \text{MgSO}_4 + \text{NH}_3 + \text{H}_2\text{O}$
- Lower Furnace Temperature
 - Decreased Oxidation Rate
- More Balanced Furnace
 - Reduced Excess Oxygen
- Reduced Slag and Iron Deposits
 - Less Catalytic SO₂ Oxidation



MOT Reduction With Targeted In-Furnace Injection TIFI

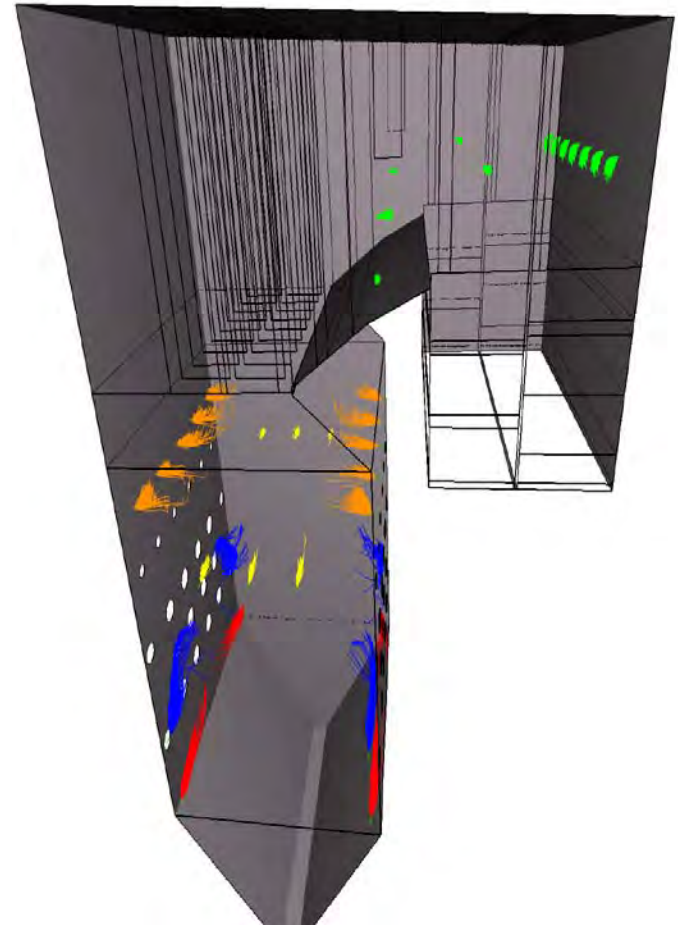
- 600 MW Wall Fired.
- Illinois Basin Coal.
- Need for Greater Low Load Flexibility.
- New Low Load Operations began Aug 2013 and continues through present.
- Original Low Load 430 MW – reduced to 275 MW

SO₃ Reduction With Targeted In-Furnace Injection TIFI



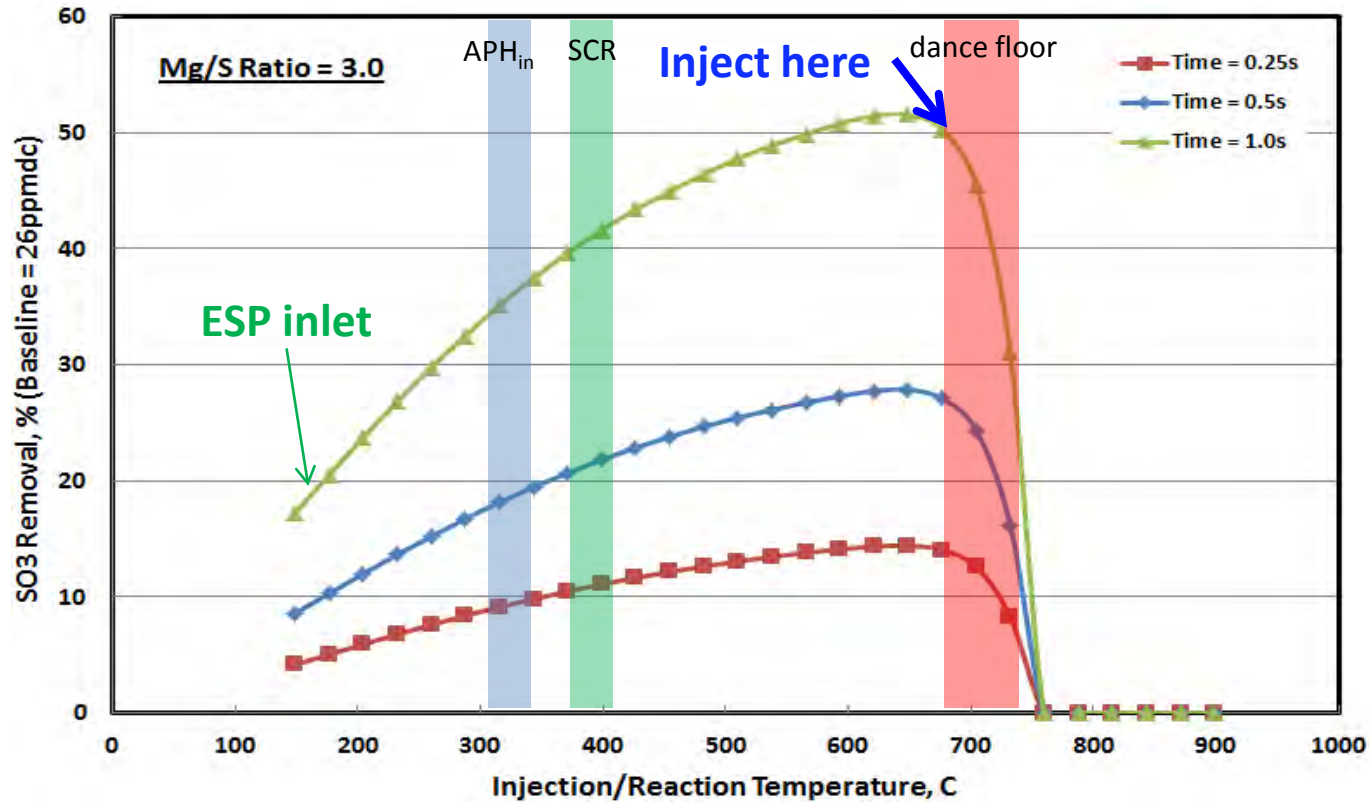
SO₃ Reduction With Targeted In-Furnace Injection TIFI

- Lower furnace injection (zones 1 – 4) is optimal for slag/fouling control
 - MgO reacts with ash to modify ash fusion temperature
 - MgO captures SO₃
- Zone 5 injection is more efficient for SO₃ control and still provides slag & fouling control at the horizontal superheats, reheats, economizer, SCR & air heater
 - MgO does not readily react with fly ash at T < 2000°F
 - Less sintering of MgO = more available surface area for SO₃

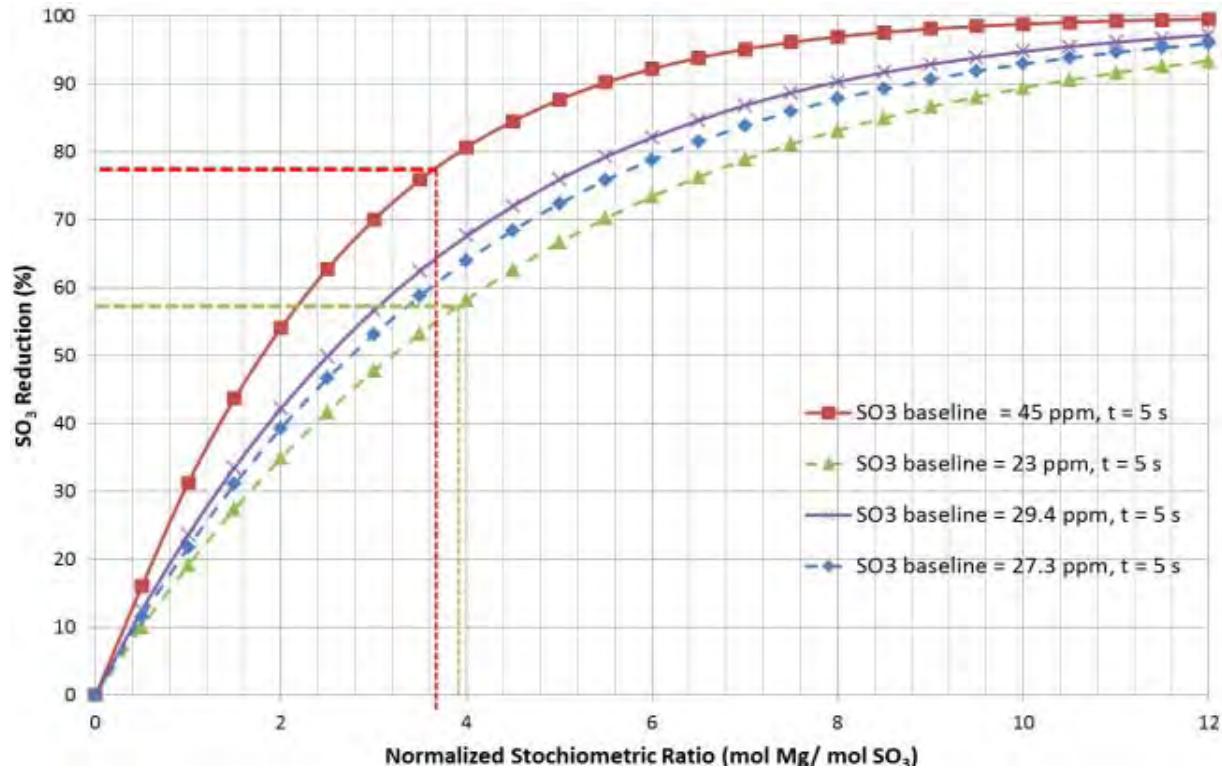


Zones 1 – 4, 5

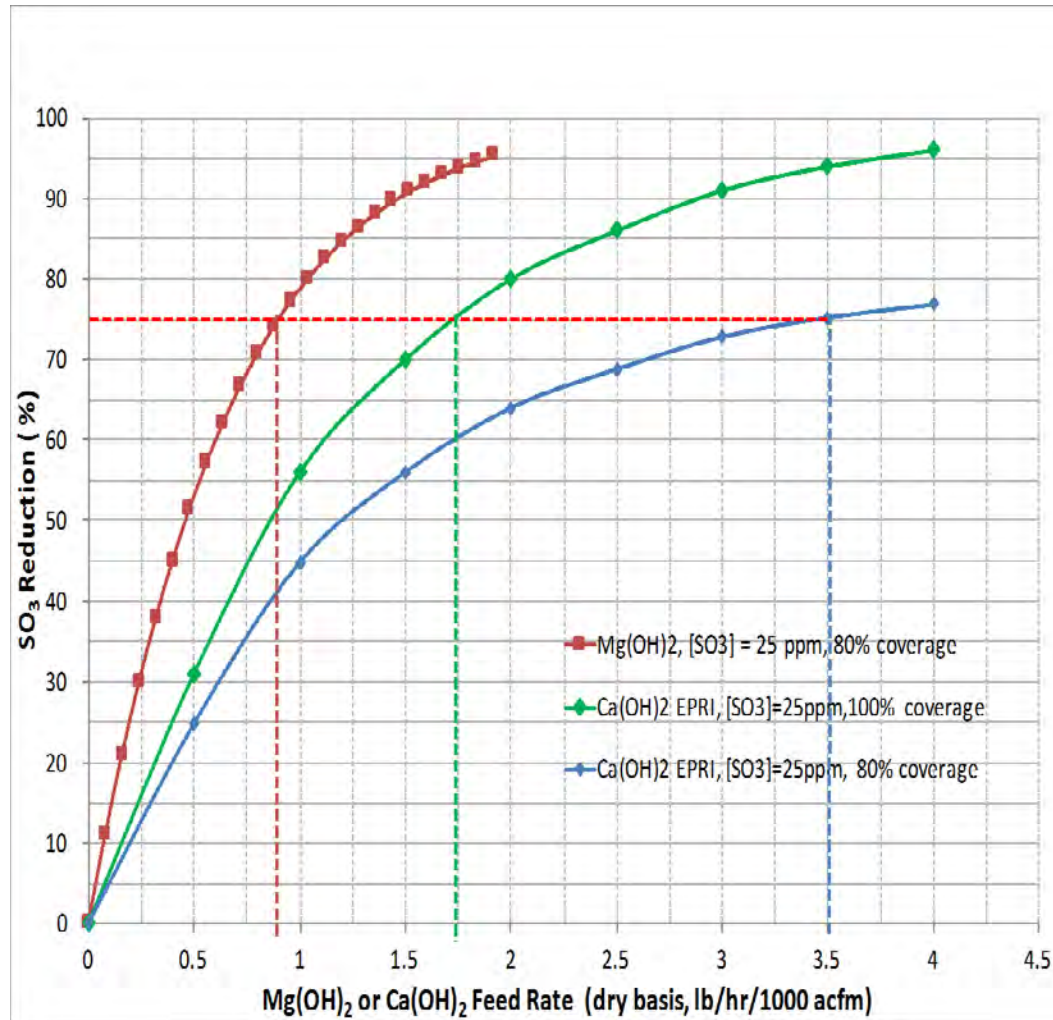
Optimized $Mg(OH)_2$ Injection for SO_3 Control



Predictive Performance Model for SO₃ Control



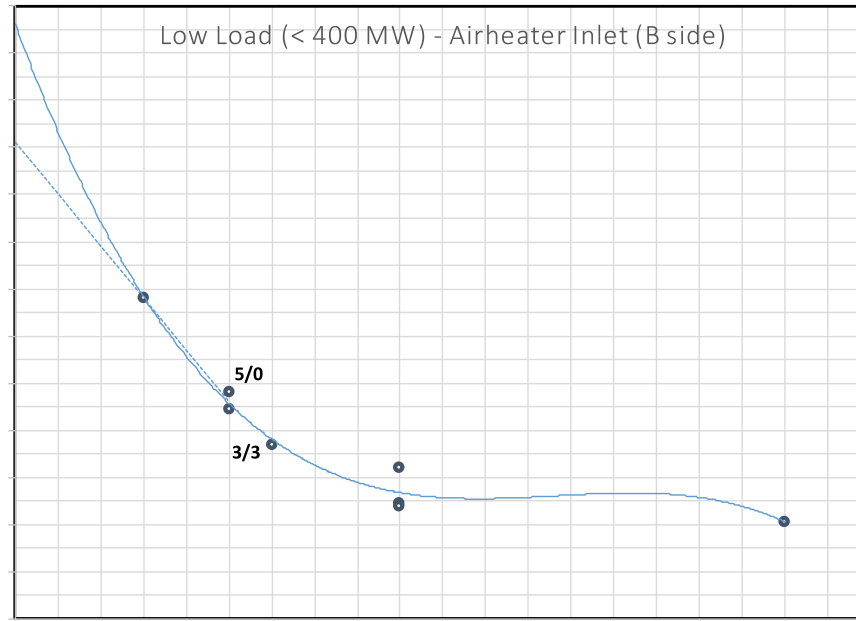
Predictive Performance Model for SO₃ Control



SO₃ Tests

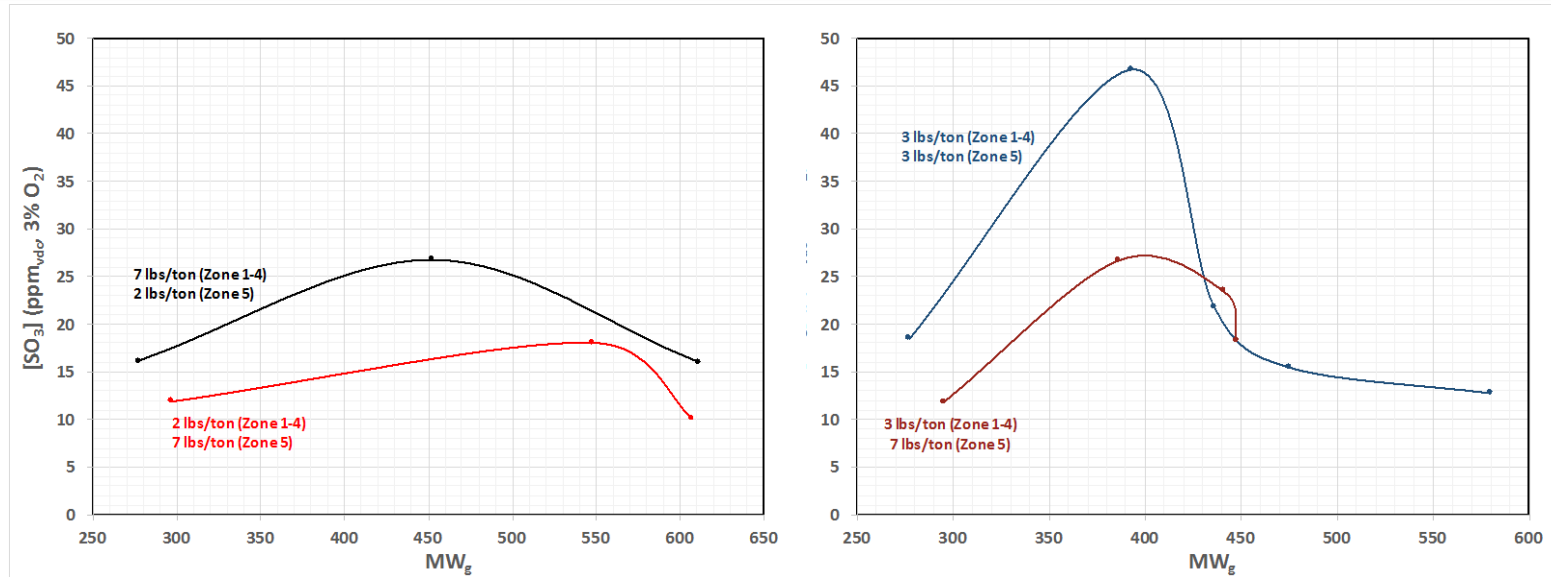
- Modified EPA Method 8A Controlled Condensate
- Single train sampling
 - Preliminary tests conducted to understand cause (dose) and effect (reduction) relationship
 - One SO₃ train measured AH inlet at low load, ramp period and full load
- Six train full test protocol July 13 -- 17
 - SO₃ measurement locations (both sides):
 - Economizer outlet
 - SCR outlet
 - APH outlet
- Unit configuration during measurements:
 - Low load
 - Ramp
 - High load
- Determined critical data on SO₂/SO₃ conversion rates, sorbent performance as a function of temperature during each unit configuration

Results at Low Load (< 400 MWg)



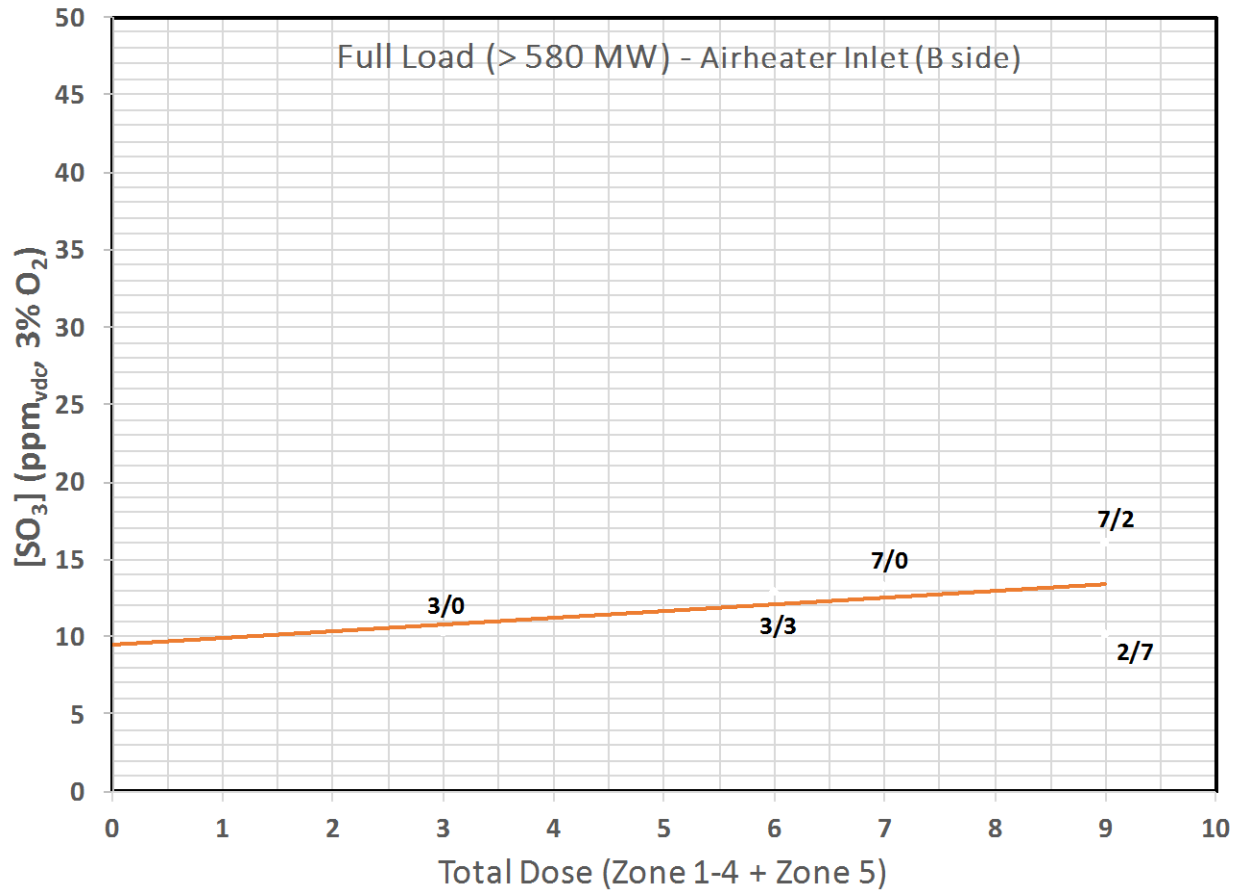
- Uncontrolled SO₃ concentration is 51 – 63 ppm_{vdc} (at 3.0% O₂)
- SO₂ concentration during this period averaged 3.66 ± 0.24 lbs/MMBtu
 - Corresponds to SO₂ = 1926 ± 125 ppm_{vdc} at 3.0% O₂
- Side B total conversion rate 2.6% -- 3.5%
 - Side B O₂'s are approximately 1 -- 2% lower than Side A
 - Therefore Side A conversion is expected to be greater than Side B

Results During Ramp



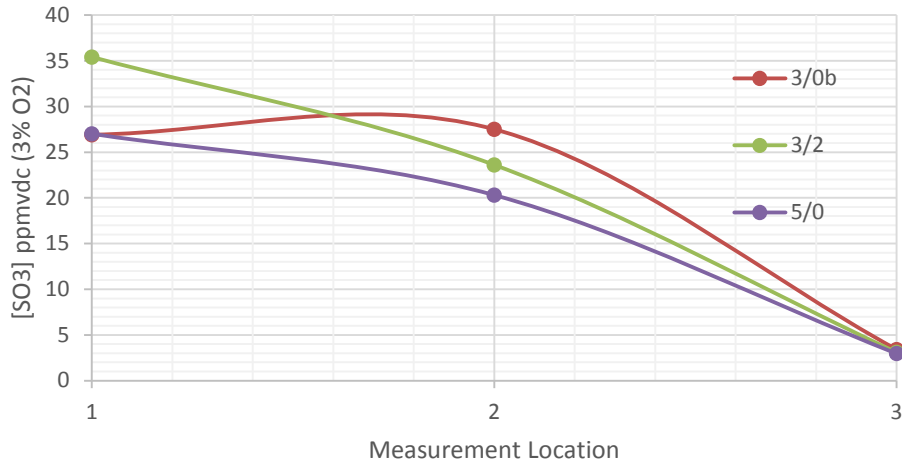
- As unit ramps, the catalyst releases stored SO_3 .
- Increasing $Mg(OH)_2$ feed rate in zone 5 during ramp decreases severity of “burn off”.
- Dance floor injection (zones 5) is 20% -- 30% more efficient than furnace injection for SO_3 control.

Results at Full Load

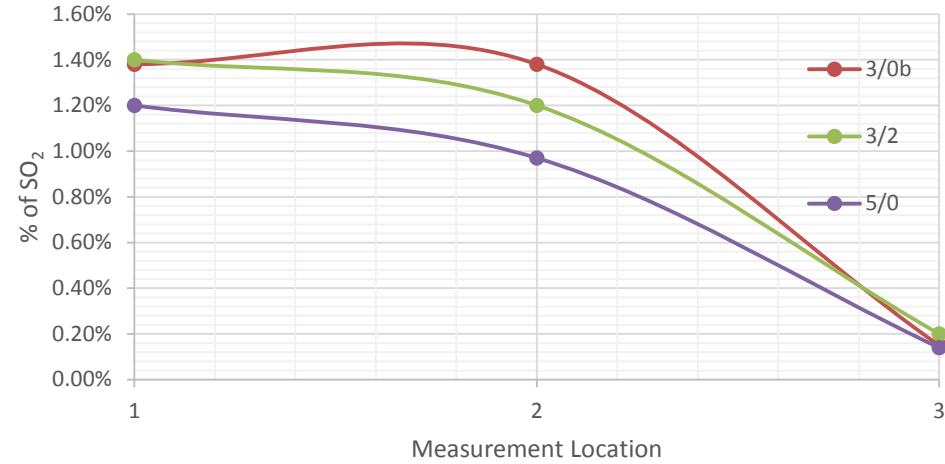


Low Load Results

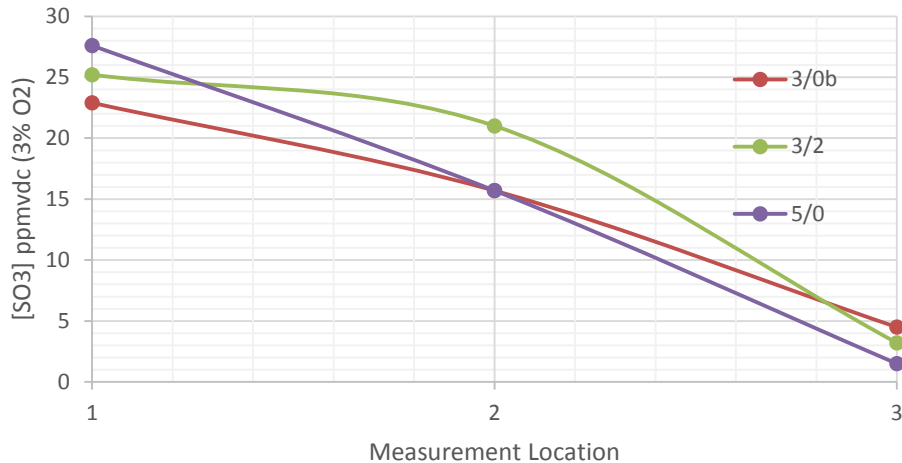
Low Load - A side



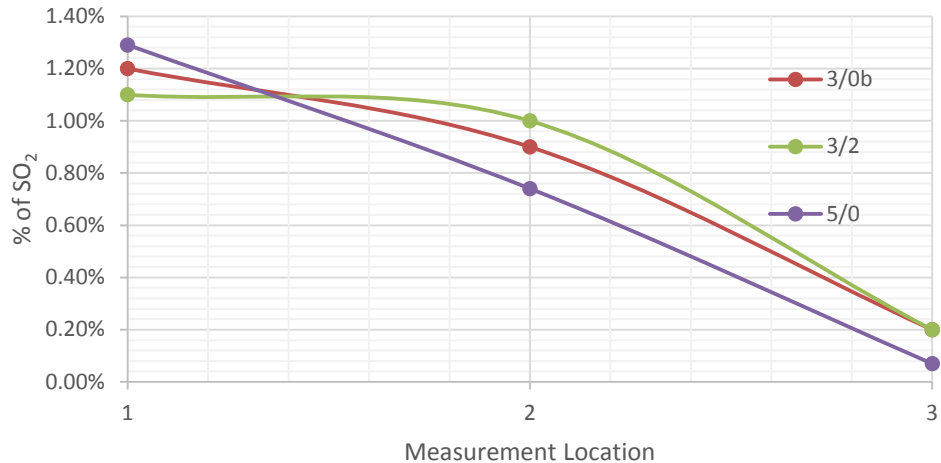
Low Load - A side



Low Load - B side

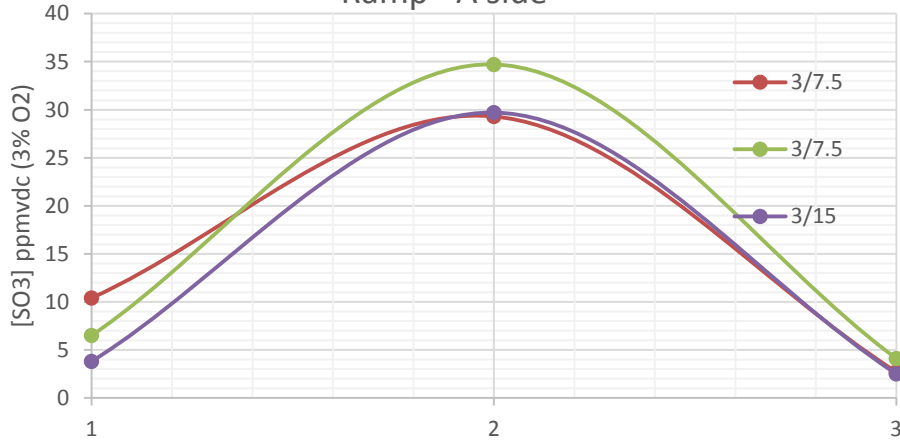


Low Load - B side

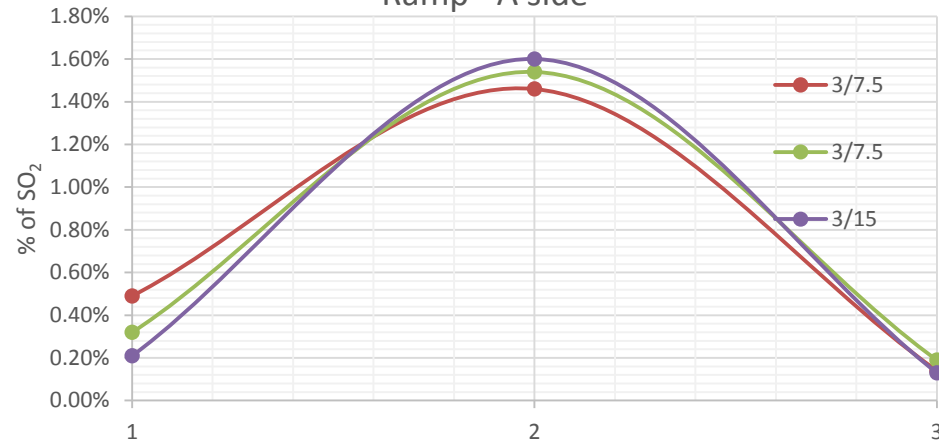


Ramp Results

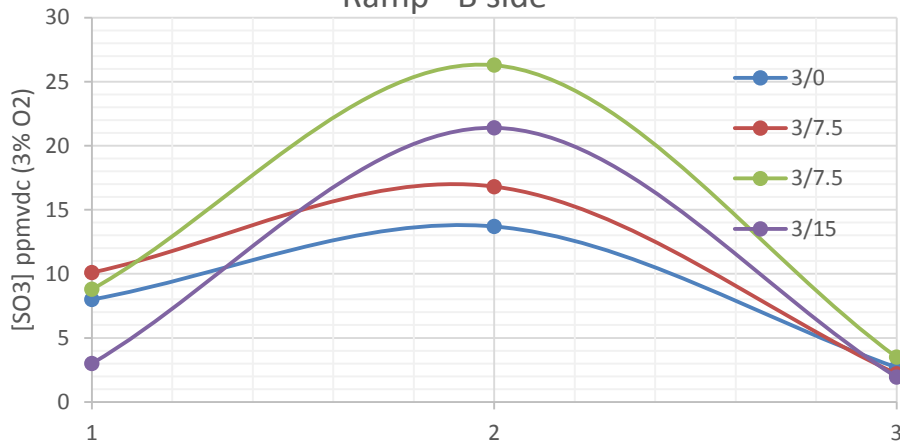
Ramp - A side



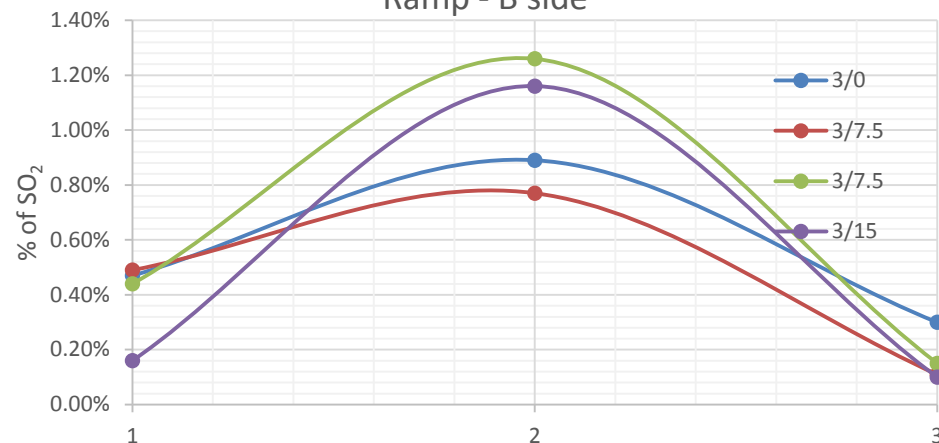
Ramp - A side



Ramp - B side

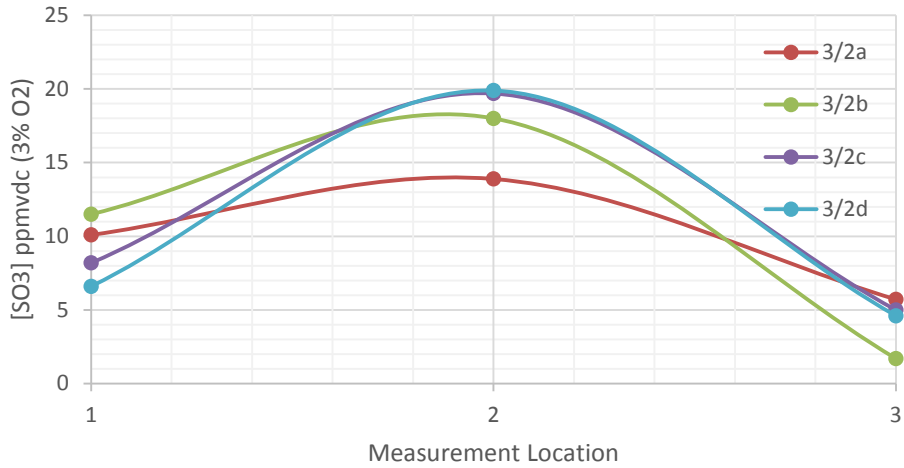


Ramp - B side

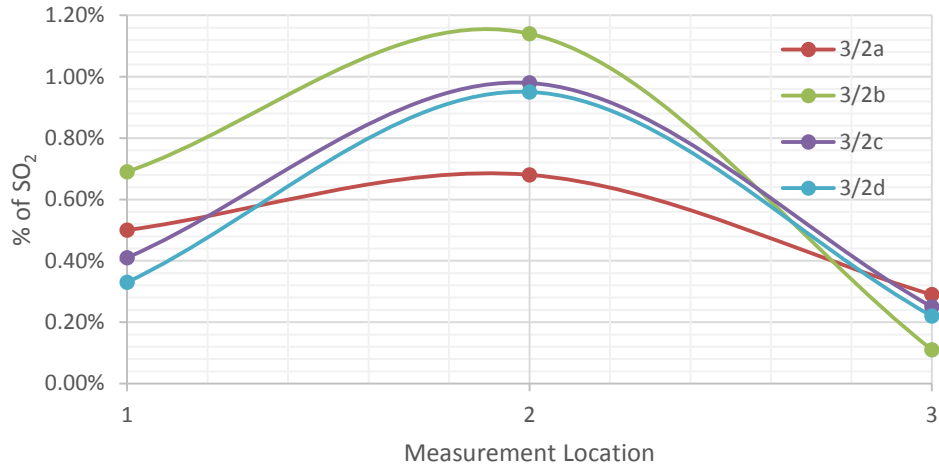


Full Load Results

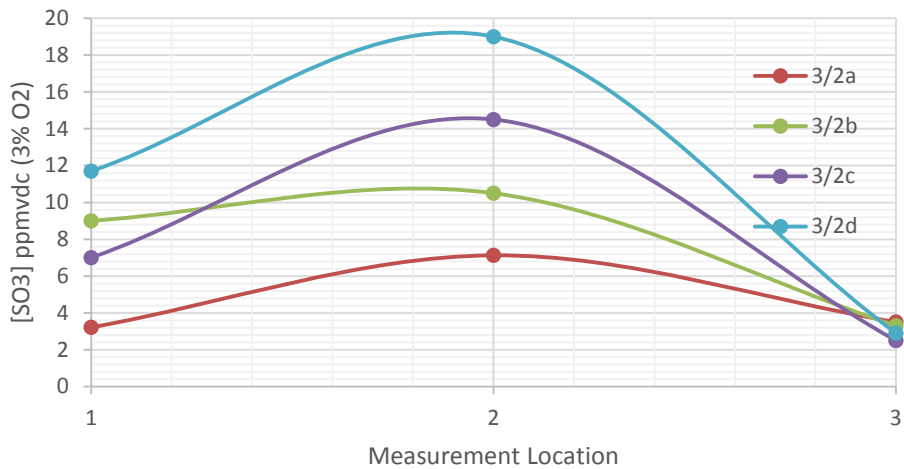
Full Load - A side



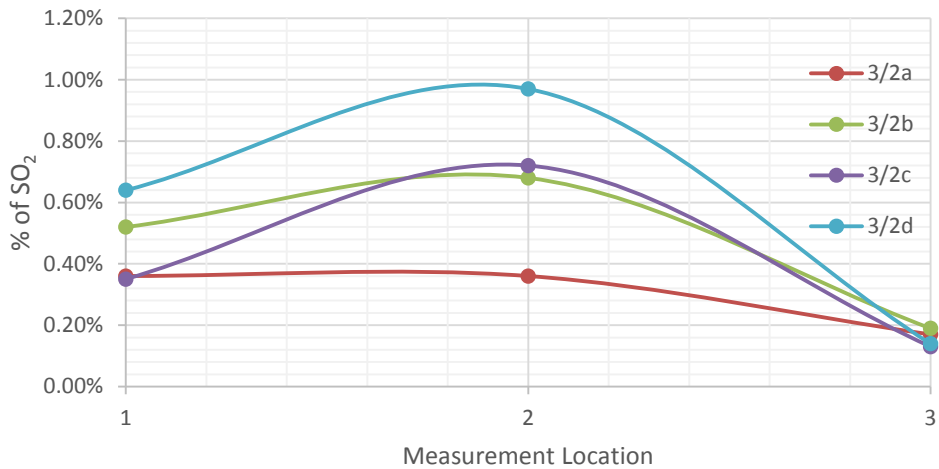
Full Load - A side



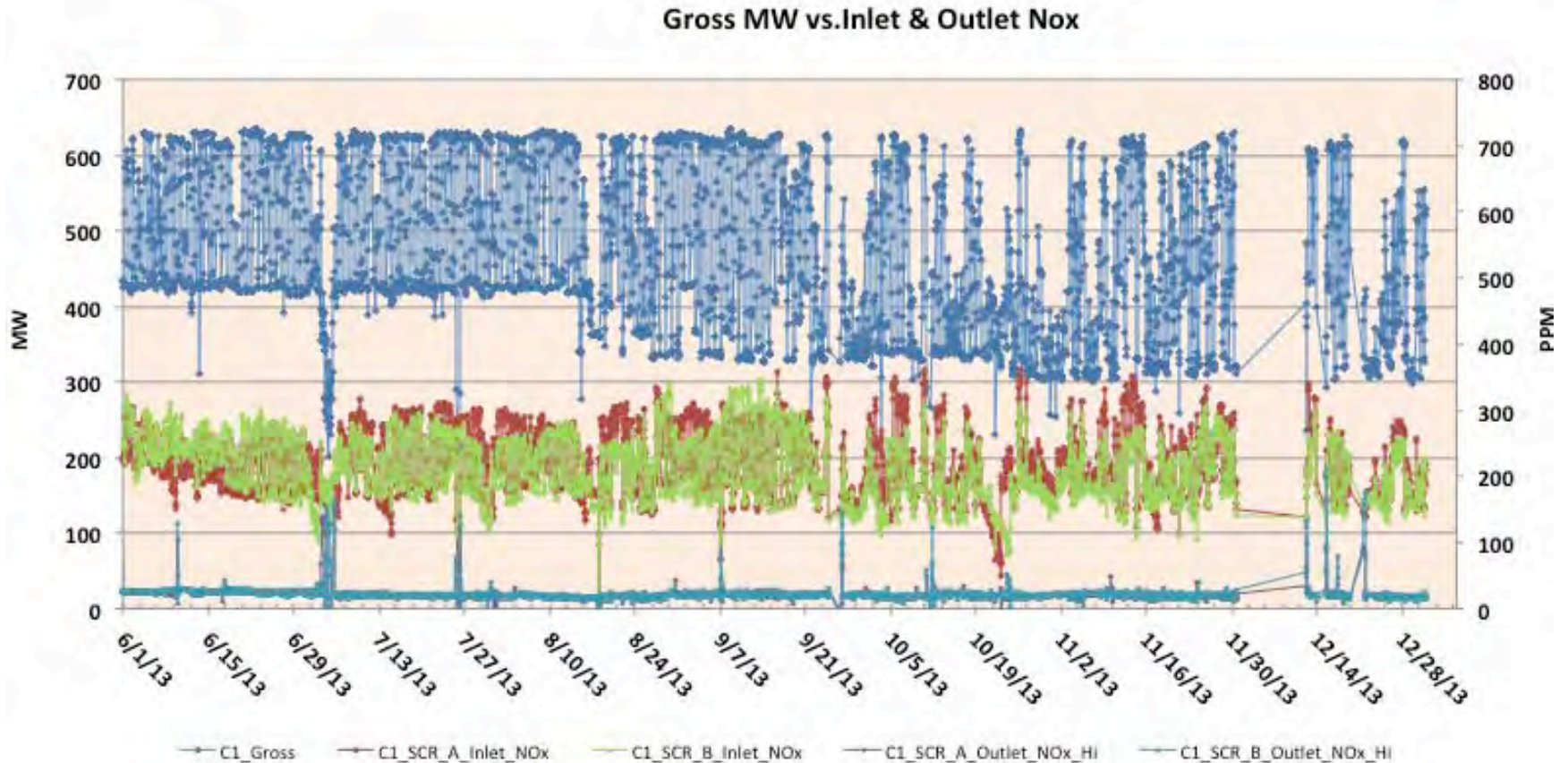
Full Load - B side



Full Load - B side



New Minimum Loads



- New limiting load factor – combustion stability
- Wider operating range may pay for all day chemical consumption

Additional Solutions

- Duct burner to raise the temperature
 - Pro: Provides the entire load range
 - Con: Economics
- Gas co-firing
 - Reduces SO_3 and NO_x concentration in the flue gas
- Burner improvements to reduce the NO_x concentration
- SNCR to reduce the NO_x concentration
- Waterside economizer bypass

Conclusions

- Several options are available to broaden the SCR operating range.
- Precise definition of low load operating conditions is mandatory.
- Operation below MOT can be detrimental if there is no mechanism to preclude ABS formation in the air pre heater.
- Economic evaluation important for optimized solution.
- TIFI is a solution especially for high sulfur applications to reduce SO_3 and broaden the operating range.

Thank You

Questions?